



A HANDBOOK FOR
ENGINEERING STUDENTS, MERCHANTS
AND USERS OF IRON AND STEEL

BY

H. R. HEARSON, M.I.MECH.E.

KIANGNAN ARSENAL, SHANGHAI, CHINA

TWENTY-ONE ILLUSTRATIONS



London
E. & F. N. SPON, Ltd., 57 HAYMARKET

Hew Pork

SPON & CHAMBERLAIN, 123 LIBERTY STREET

1912

CONTENTS

OHAP'				PAGE Vii
	LIST OF ILLUSTRATIONS	•	•	VII
	PREFACE			ix
I.	CHEMICAL ELEMENTS IN IRON AND STEEL .			1
II.	IRON ORES			6
III.	THE BLAST FURNACE			9
IV.	THE MANUFACTURE OF WROUGHT 1RON .			2 2
v.	THE MANUFACTURE OF STREE	•		27
VI.	THE SIEMENS-MARTIN OR OPEN-HEARTH PROCESS			38
VII.	THE BASIC OPEN-HEARTH PROCESS	•		50
VIII.	THE ACID BESSEMER PROCESS			58
IX.	THE BASIC BESSEMER PROCESS			66
X.	THE TREATMENT OF STEEL INGOTS .			76
XI.	EFFECTS OF ADDING OTHER METALS TO STEEL		•	85
XII.	MECHANICAL TESTING OF STEEL			88
XIII.	HEAT TREATMENT OF STEEL			9
	THINK			109

LIST OF ILLUSTRATIONS

FIGURE						PAGE
1. Calcining Kiln				•		8
2. Blast Furnace	•					10
3. Tuyere .						11
4. Hot-blast Stove	•					13
5. ,, ,, ,,						14
6. Puddling Furnace	з.				• .	24
7. Cementation Fur	nace					29
8. Crucible SteelM	lelting	Hole				31
9. Gas Producer	•	•	•			39
10. Siemens' Open-he	earth Fu	rnace				40
11. Furnace Lining-	-Basic N	M aterial				52
12. Bessemer Conver	ter					60
13. Charging the Cor	verter					61
14. Steel Ingot						77
15. Soaking Pits				•		79
16. Ingot Mould for	Fluid C	ompress	ion			81
17. Effects of Hamm	ering, R	Colling, a	nd Pr	essing		84
18. Testing Steel S	ess Di	agram				90
19. Flat Test-piece						93
20. Test-piece—Circu	ılar Sec	tion		•		93
91 That for Wolding						96

PREFACE

THE following, by kind permission of the editor, is extracted from an article entitled "The Influence of Iron on World Power," published in the London Daily Telegraph of 8th January 1912. "The three greatest World Powers of the present day are the greatest makers of iron and steel. These nations Great Britain, Germany, and America. lesson of the records of the past is that the peoples which made the most iron and steel had the greatest influence on the History of their times. About 2000 years ago the Roman Empire was all-powerful; in that Empire was made more iron than in all the other nations of the world put together. In the sixteenth century the greatest iron-making nations were Spain, France, and England, and these were then the three most powerful countries. The Romans carried into Spain the knowledge of working iron and steel; and the forges of Catalonia, and the armour of Castile, enabled a few Spaniards to seize the riches of other countries which had reached a high state of civilisation, but knew not the methods of manufacture of iron. Germany has risen rapidly as a World Power synchronically with the

enormous increase in the output of her iron and steel. It is not necessarily the country in which the greatest quantity of iron ore is found that wields great influence: it is the country which manufactures iron and steel from the ore. Northern Africa has had vast deposits of iron ore, but it has always been exported. Canada is a land where iron ore is found in abundance, where furnaces and forges are rising up. The potentialities of that country are wonderful, because of those furnaces; not of its cornfields and orchards-important though they are—but because of the manufacture of steel, which is necessary for the construction of fleets of ships and thousands of miles of railroads. There is another country, the speculation on whose future is as attractive, and whose past History is far more wonderful than that of Canada. That country is China. the slumbering country, is now awake; and what is of more importance, China contains iron ore. Napoleon trusted to big battalions; it was his great generalship which enabled him to bring up his big battalions, and they won-guns, armour, and courage being equal. Courage, admirable as it is, will not prevail against guns and armour and numbers. It the great Eastern nation works its iron and steel as other nations have done—and there is every reason to suppose that China will do so-then the future will reveal some extraordinary changes in the might of that country as now compared with that of other great World Powers."

The object of this book is to give a brief and simple

outline of the principal operations in connection with the manufacture of iron and steel. Some information concerning this great industry may be interesting to all, and useful to those commercially connected with iron and steel. Engineering students who have opportunities of seeing iron and steel manufactured may find that this outline will enable them to understand easily the work that is going on whereby they can then quickly acquire a practical knowledge.

Instead of giving all definitions at the beginning, technical expressions are used where necessary, and then defined at the point where it seems most appropriate. Therefore, it is recommended that this book be read through quickly at first, in order to obtain a general idea of its contents.

H. R. HEARSON.

CHAPTER I

CHEMICAL ELEMENTS IN IRON AND STEEL

An element is a substance which cannot be divided into other substances. There are about 80 elements, and more are constantly being discovered. Each metal in its pure state is an element, and no one metal can be changed into another metal. For example, copper cannot be changed into tin or any other metal, tin cannot be changed into copper; but if copper and tin are melted together they form an alloy which is brass. This alloy has properties different from either copper or tin.

There are other elements which are not metals, such as carbon, which is the chief component of all substances that are ambustible. Coal and wood are composed chiefly of carbon. Oxygen is an element; it is a gas, which, mechanically mixed with nitrogen gas, forms our atmosphere.

A chemical compound is a substance formed by the chemical combination of two or more elements. For example, the elements oxygen gas and hydrogen gas combine chemically and form water.

1

Chemical combination takes place in definite proportions of elements, a definite number of atoms of one element entering into chemical combination with a definite number of atoms of another element.

Each element has a definite value with regard to each other element; the relative values are called the *atomic weights* of the elements.

The atomic weights of oxygen and hydrogen are:-Oxygen, 16; hydrogen, 1. These gases will only unite with each other in the proportion of 16 to 1, by weight. The formula of water is H₂O; this means that it is composed of two parts, by weight, of hydrogen, and one part, by weight, of oxygen; so 2 lbs. of hydrogen will chemically combine with 16 lbs. of oxygen to form 18 lbs. of water. Two lbs. of hydrogen will not chemically combine with 13, 14, or 15 lbs. of oxygen; if, say, 2 lbs. of hydrogen is mixed with 14 lbs. of oxygen, and a lighted match be applied to the mixture, the 14 lbs. of oxygen will combine with $2 \times \frac{14}{16}$ lbs. (= $1\frac{3}{4}$ lbs.) of hydrogen, and $15\frac{3}{4}$ lbs. of water will be formed: the remaining $\frac{1}{4}$ lb. of hydrogen will be in a free state as a gas. The principal elements, with their symbols and atomic weights, to be considered in the manufacture of iron and steel are:-

	Nam	e.	Sy	mbol.	Atomic Weight.
1	Iron			Fe	56
	Manganese .			Mn	55 、
	Aluminium .			Al	27.5
	Magnesium .			Mg	24
Metals {	Nickel .			Ni	59
	Chromium .			\mathbf{Cr}	`52.5
	Vanadium .			\mathbf{v}	51.25
	Titanium .			Ti	50
	Tungsten or	Wolfram		W	184

*Name.		S	ymbol.	Atomic Weight.
Carbon			C	12
Oxygen			0	16
Hydrogen			Π	1
Nitrogen			N	14
Silicon			Si	28
Phosphorus			P	31
Sulphur			S	32
Calcium			Ca	40

Iron (Latin name, Ferrum) quickly combines with oxygen to form oxide of iron.

The three oxides of iron are:-

Ferrous oxide.—A chemical compound of iron and oxygen in the proportion of one atom of iron to one atom of oxygen, represented by the formula FeO. If there is any moisture in the air, iron will be attacked by the oxygen, and ferrous oxide or rust will be formed on the iron.

Ferric oxide.—The combination of 2 atoms of iron with 3 atoms of oxygen, represented by the formula Fe₂O₃.

Magnetic oxide.—The combination of 3 atoms of iron with 4 atoms of oxygen, represented by the formula Fe₃O₄.

If ferrous oxide is made to absorb more oxygen, it is converted into ferric oxide.

If ferric exide is heated, oxygen gas is given off and it changes to magnetic oxide.

Manganese is a metal which is always one of the chemical components of iron and steel. As it easily combines with oxygen, and to some extent with sulphur, it is useful in the manufacture of steel.

Carbon and oxygen enter into chemical combination with each other to form the gas called carbon monoxide

(CO), or the gas carbon dioxide (CO₂), the usual name of which is carbonic acid gas.

When fuel is consumed in a furnace in which there is a plentiful supply of air, the carbon of the fuel combines with the oxygen in the air and forms CO_2 ; if the air supply is insufficient, the CO_2 , on coming into contact with more hot carbon, takes up one more atom of carbon and becomes C_2O_2 , or 2CO.

Such chemical actions are conveniently represented by equations:—

$$C + O_2 = CO_2$$
.
Carbon and oxygen form carbon dioxide.

$$CO_2$$
 + C = C_2O_2 = $2CO$.

Carbon dioxide and carbon form carbon monoxide.

All fuel is composed chiefly of carbon, hydrogen, and compounds of hydrogen and carbon called "hydrocarbons."

An element is said to be "oxidised" when it combines with oxygen to form a chemical compound.

A chemical compound containing oxygen is said to be "deoxidised" when it is made to give up its oxygen.

Silicon is easily oxidised. When oxidised it is called silica, which has the formula SiQ. Silica is the most plentiful of all substances.

Pure white sand is an example of silica. All iron ores contain silica, and in the manufacture of iron the silica gives up its oxygen and becomes silicon. The greater part of the silicon is removed, but a portion remains as a component of the iron.

The worst impurities in iron are *phosphorus* and sulphur.

Too great a proportion of phosphorus makes iron and steel brittle when cold; it is then said to be "cold short."

Too great a proportion of sulphur makes iron and steel brittle when red-hot; it is then said to be "red short."

CHAPTER II

IRON ORES

ORES which are found near the surface of the earth are "quarried," and ores at lower depths are "mined."

Iron ore is made up of oxide of iron and other substances, which in most cases consist chiefly of silica and clay. The "other substances" are the gangue of the ore, and the process of smelting separates the gangue from the iron.

The three classes of ores are:—Ferrous ores, ferric ores, and ferrous-ferric ores. They all contain phosphorus.

Ferrous ore, of which Cleveland Ironstone is an example, contains iron in the form of ferrous oxide combined with carbon, forming ferrous carbonate (FeO,CO₂).

Ferric ore, such as English hematite, red and brown, contains iron in the form of ferric oxide.

Ferrous-ferric ore has the highest percentage of iron; it consists almost entirely of ferrous oxide and ferric oxide. The ore called magnetite is the most plentiful of this class, and it is found principally in Sweden.

PREPARATION OF ORES FOR SMELTING

A'll ferrous ores are heated by the process called calcination before being smelted. Calcination changes the ferrous oxide into ferric oxide; carbon dioxide and moisture are driven off and other small chemical changes take place.

Advantages of calcination.—Ferric oxide is easier to smelt in the blast furnace than ferrous oxide, as it does not enter into chemical combination with the silica in the ore.

The driving off of the carbon dioxide has two advantages; by containing a lesser quantity of this gas, the gases generated in the blast furnace burn with a greater heat, and the gases after they leave the furnace are better for producing power in gas engines, etc.

Calcination makes the ore porous, so that it is more quickly melted in the blast furnace by the heat passing more easily through it.

Calcination causes a shrinkage of the ore, but the weight of iron contained in it remains the same; thus a blast furnace can contain a greater weight of calcined ore, and more iron can be smelted.

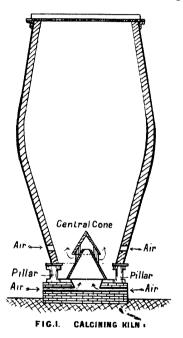
Brown hematite was are sometimes calcined to drive off the water and a little carbon dioxide which they contain.

Red hematite ores are not calcined.

Ores may be calcined in open heaps on the ground, but it is more economical in the consumption of fuel and in the labour of handling the materials that calcination be conducted in kilns.

• Fig. 1 is a section of a calcining kiln built of steel

plates and lined with firebricks. A fire is first lighted at the bottom, and ore and fuel are then charged from the top. The fuel used is small coal, and as there is no forced draught or chimney, it burns very slowly. Very little fuel is needed, as additional heat is generated by



the chemical action of the ferrous oxide being changed to ferric oxide. The calcined ore is withdrawn through openings between the pillars at the bottom of the kiln.

Air is required for the combustion of the fuel and for the oxidation of the ferrous oxide; it is admitted through holes at the bottom, between the pillars, and up through a central cone.

CHAPTER III

THE BLAST FURNACE

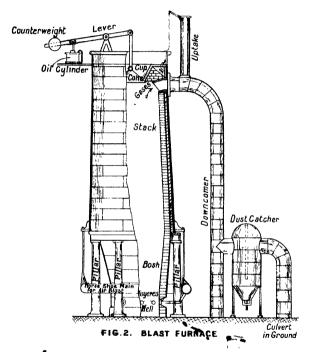
The process known as "smelting" is conducted in the blast furnace at a very high temperature. The ore is converted into pig iron, slag, and gases. Fig. 2 is a sketch, partly in section, of an iron-smelting blast furnace. It is built of steel plates and lined with firebricks. The whole is supported on cast-iron pillars. Internally, the furnace consists of the cylindrical "well" or "hearth" of brickwork, at the bottom; next to this is the lower cone which is called the "bosh," the upper cone is the "stack."

Ore and fuel are charged from the top of the furnace, and the stack expands in diameter from the top to the bottom to allow them to become loose as they descend.

The furnace is the contracted in diameter by the bosh so the materials may be held up until the fuel is consumed at the bottom of the bosh. The melted iron and slag continually drop into the well of the furnace, from which they are tapped out.

- A furnace is "tapped" by removing a fireclay plug from a hole which is called the "tap hole"; mosten iron then flows out.
 - · After smelting, there is a residue from the ore, which ·

is called "slag"; this, being of lower density—that is, lighter—than iron, floats on top of the iron, and it is tapped out of the furnace through a hole called the "slag hole" near the top of the well.



The materials are charged into the furnace by means of a cup and cone. When the lever which supports the cone is released, the weight of the materials causes the cone to descend, and when these are discharged into the furnace the cone is raised by a counterweight at the end of the lever. A rod is connected from the lever to a piston which works in a cylinder containing oil;

a pipe connects the two ends of the cylinder so that oil can flow from one side of the piston to the other. The oil prevents the lever from being suddenly raised or lowered. If the cone closes with a bang on to the cup, the iron castings of which they are made may be cracked.

The air blast enters the furnace from the brick-lined, horseshoe main through tuyeres built into the brickwork at regular intervals at the top of the well.

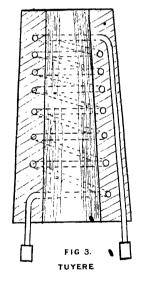
The combustion of the fuel and the reduction of the ore generate a large quantity of gases, which are collected at the top of the stack and passed into a large brick-lined tube called the downcomer, thence through

the dust catcher to culverts which lead them to where they are required for further use.

The dust catcher collects the dust which is blown out of the furnace with the gases; if the gases are to be used in a gas engine, it is very necessary that the dust be first separated from them.

As the tuyeres are exposed to the heat of the arrace, means must a taken to prevent the iron of which they are made from melting.

There are many kinds of tnyeres; one kind is shown



in fig. 3. This consists of a tapering spiral coil of wrought-iron pipe, 1 inch diameter, with cast iron moulded around it.

When in use, water is made to flow through the coil; the water carries away the heat so quickly that the cast iron cannot melt.

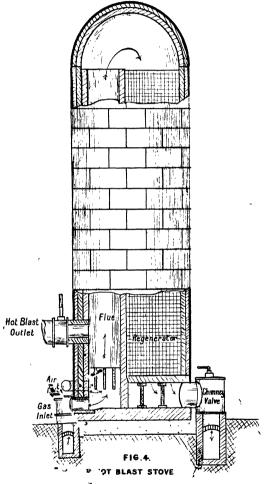
Size of blast furnaces.—Furnaces of large capacity work with the best economy. A high furnace requires less fuel per ton of ore reduced than does a low furnace, but a furnace should not be higher than 90 feet, as, if higher, the fuel will be crushed by the weight of the ore.

The maximum internal diameter at the top of the bosh should not exceed 22 feet; if of greater diameter, the air blast will not get through the burning materials to the centre.

Hot-blast store.—An economy of fuel is obtained by heating the air before it is blown into the furnace. Fig. 4 is a sectional elevation, and fig. 5 is a sectional plan of a hot-blast stove, built of steel plates, lined with fire bricks, and worked on the "regenerative" system. Gases from a blast furnace are ignited in a vertical flue of elliptical section. Divisions are made in the lower part of the flue to split the gases into sheets, so that they burn more readily. To assist combustion, air is admitted just above the gas inlet and mixes with the gases in the flue. Long flames go up the flue, and the hot products of combustion pass down to regenerator to the claimney valve.

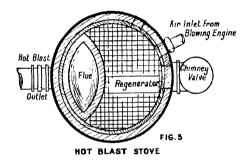
The regenerator is a chamber fixed with checkered bricks, that is, the bricks are laid in such a way as to expose as much of their surfaces as possible to receive and give forth heat, while, at the same time, allowing free passage for gas or for air. When the regenerator has become greatly heated, the gas and air inlet valves

and the chimney valve are shut. The air-blast inlet



he hot-blast outlewalves are then opened and cold air from the blowi, engine is admitted at the

bottom of the regenerator. The air passes up between the hot bricks and down the flue to the hot-blast outlet, and thence, at a temperature of about 1500° F., to the blast furnace. In the meantime, the gases from the blast furnace are being burnt in a second hot-blast stove, and when the first stove is cooled down so that the air comes out of it at a temperature of about 1100° F., the valves are reversed. The first stove is then reheated and cold air is heated in the second stove.



Hot-blast stoves are worked in pairs or in sets of three.

Blowing engines are large air pumps which co fress air and force it under pressure to the air-blatinain. They are now generally driven by gas e the engines being worked by the gases from the blast furnace.

Working the Blast Fu RNACE

Fuel.—Coal or coke is used as fi el according to the prices at which each may be obtained. Bitum inous coal is either coking or non-coking. If it is suitable for coking, it is coked for use in the blast furnace. If it is

15 a DE A

THE BLAST FURNACE

not suitable, it is used without coking. Anthracite coal may also be used. Coke is better than coal as fuel for a blast furnace; it burns with a more intense heat, and it is not so easily crushed as coal is.

100 parts of bituminous coal may have an analysis approximately as follows:—Fixed carbon, 55 parts; hydrocarbons, etc., 35 parts; water, 5 parts; and ash, 5 parts.

Coke is obtained by highly heating bituminous coal without or with very little admission of air. Water and the free hydrocarbons of the coal are driven off. The coke thus obtained contains a greater percentage of carbon than the original coal. Good coke has a silvery appearance. It should be dense, but also porous; that is to say, the pores should be very small, otherwise the coke will not be strong and it will be easily crushed in the furnace. The pores allow the heat to pass through the coke, so that it burns quickly and with an intense heat.

Flux.—A flux is a substance which is added to other substances to cause them to become fluid when heated. It must be of such chemical composition that it will, when heated, enter into chemical combination with the substances which are to be fluxed. It is necessary to form from the gangue a liquid slag which may be tapped from the furnace.

Ores which contain a large percentage of silica require a flux, as silica does not melt at the temperature of the blast furnace.

Limestone is charged into the furnace as a flux; it contains calcic carbonate (CaO,CO₂). The CO₂ at once escapes with the blast-furnace gases, and the lime

(CaO), which is left, chemically combines with the silica to form calcic silicate (2CaO,SiO₂), usually called silicate of lime, the melting point of which is below the temperature of the blast furnace.

If alumina (Al₂O₃) is present in the ore with the silica, the addition of limestone as a flux forms a compound silicate of lime and alumina, which melts at a lower temperature than calcic silicate.

Some ores are called "self-fluxing"; this means that they contain a sufficient quantity of lime to combine with the silica.

Some ores contain more lime than is required to assist in the melting of the silica; such ores can be mixed with "non-fluxing" ores, and no limestone flux will be needed. For example, one kind of ore may contain 20 per cent. of silica and alumina and 4 per cent. of lime; this is a non-fluxing ore. Another kind of ore may contain 10 per cent. of silica and alumina and 18 per cent. of lime; this is a self-fluxing ore which contains more lime than is required. If these two kinds of ore mixed together are charged into the blast furnace, they will be self-fluxing.

The charge is the total of materials which are put or "charged" into the furnace. The charge consists of the ore, the flux, and the fuel; the ore and the flux are the burden of the furnace, and the fuel supports the burden. The greater the burden that the fuel is capable of supporting, the greater will be the output of pig iron from the furnace per ton of fuel used.

Reduction of the ore.—When the air blast on entering the furnace meets the burning fuel, the expegen of the air enters into chemical union with the

combustible elements in the fuel and produces a high-temperature. CO gas is first produced, and this taker oxygen from the oxides in the ore to form CO₂. The transferring of oxygen is called *reduction*, and the oxide which gives up its oxygen is said to be reduced.

Oxide of iron is thus reduced to metallic iron, which melts and drops, together with the molten slag, into the well of the furnace.

The iron is tapped from the furnace every 6 to 8 hours, and the slag is tapped as often as is necessary.

Pig iron.—Iron as it is tapped from the furnace is known as pig iron; it is allowed to flow into moulds made in sand in front of the furnace. Each pig is about 3 feet long and weighs about 120 lbs.

Pig iron contains carbon, silicon, phosphorus, and sulphur, which have been taken up in the process of reduction from the materials in the charge. The term "cast iron" should not be confused with pig iron. Cast iron is iron which has been melted in a cupola and cast into some definite shape.

CHEMICAL ACTIONS IN A BLAST FURNACE

The chemical actions may be represented by chemical equations:—

Reduction of ferric oxide:-

$$Fe_2O_3$$
 + 3CO = 2Fe + Ferric oxide and carbon monoxide yield iron and 3CO₂.

Reduction of manganese oxide:-

$$\mathrm{Mn_3O_4}$$
 + 4CO
Manganese oxide and carbon monoxide yield
3Mn + 4CO₂.
manganese and carbon dioxide.

Reduction of phosphorus pentoxide (phosphoric acid):—

$$P_2O_5$$
 + 5CO = 2P
Phosphoric acid and carbon monoxide yield phosphorus
+ 5CO₂,
and carbon monoxide,

The silica is directly reduced by carbon, thus:—

The two equations which follow represent the chemical actions which cause the formation of slag:—

$$2\text{CaO} + \text{SiO}_2 = 2\text{CaO}, \text{SiO}_2.$$

Lime and silica yield silicate of lime.
 $2\text{AlO}_3 + 3\text{SiO}_2 = 2\text{AlO}_3, 3\text{SiO}_2.$
Alumina and silica yield silicate of alumina.

The silicate of alumina combines with six times its weight of silicate of lime to form a compound silicate of time and alumina; this compound is represented by the formula: — 2Al₂,3SiO₂+6(2CaO,SiO₂). This is the main composition of some blast-furnace slags, and it consists, approximately, of silica, 38 per cent.; alumina, 14½ per cent.; and lime, 47½ per cent.

Uses of blast-furnace slag.—Slag may be used instead of stone for road-making and for railway ballast. It may be made into cement or bricks. Slag wool (an insulating material) is also made from it (see pp. 49, 55, 65).

QUALITY OF PIG IRON

In the selection of a pig iron for any purpose, the quantity of phosphorus which it contains is generally the most important consideration. Nearly all the phosphorus in a blast-furnace charge goes into the pig iron. If a pig iron with a small percentage of phosphorus is required, ore, fuel, and flux, which contain little phosphorus, must, if easily procurable, be selected.

The following table shows the composition of some pig irons:—

Component Parts.	Clevela	Hematite or Acid Bessemer.	Swedish Magnetite.	Basic Bessemer.
Phosphorus .	1.60	0.05	0 03	3.00
Graphitic carbon	3.20	3.42	2.00	0.50
Combined carbon	0.50	0.46	2.00	2.80
Silicon	2.60	2.20	1.20	0.20
Sulphur	0.08	0.04	0.01	0.07
Manganese .	0.60	0 47	3.00	2.00
Iron	. 91.42	93.36	91.76	▶91.13
	100.00	100.00	100.00	100,00

Grey and white pig iron.—A blast furnace which is working with a light burden, or at a high temperature, generally produces a grey pig iron, which contains

20

much carbon and silicon, most of the carbon being graphitic carbon.

If the burden of the furnace is heavy and at a comparatively low temperature, a white pig iron is produced; this contains less carbon and silicon, and most of the carbon is combined carbon.

Carbon is a component of pig iron in two states—as combined carbon and as graphitic carbon. As graphitic carbon it is not in chemical union with any other element in the iron: it is in a free state in the form of The other chief differences between grev pig iron and white pig iron are: - Grey pig iron contains more manganese and less sulphur, is more fluid when melted, expands when changing from a fluid to a solid, has a coarse grain, and is comparatively soft and tough.

White pig iron becomes of a pasty condition when below its melting-point; this condition is unfavourable for making a clean, smooth iron casting, but it is favourable for "puddling" in the manufacture of wrought iron. White pig iron is fine-grained, hard, and brittle.

To understand what is meant by the "grain" of a metal, break a piece of wrought iron and a piece of porcelain and compare the fractures. The former has a coarse, fibrous grain; the latter has the finest possible grain.

Grey pig iron has a coarse graip, but not a fibrous grain.

BLAST-FURNACE GASES ...

Great volumes of gases of many different lands mixed together are generated in a blast furnace.

The following table shows what the gases consist of, and their approximate relative proportions:—

Gas.	Chemical Formula.	Furnace with Coal Fuel.	Furnace with Coke Fuel.
Combustible— Carbon monoxide . Hydrogen	C O H	28	29
Methane, or Marsh gas	CH	5	
Incombustible— Carbon dioxide	CO	9	15
Nitrogen (from the air)	N 2	52	55
		100	100

The gases after leaving the blast furnace undergo a distilling process called "scrubbing," in order to recover the ammonia and tar contained in them. The scrubbed gases are then used for steam raising by burning them in boilers with special furnaces and long flues: or power is generated by using the gases direct in a gas engine. About three times as much power may be obtained by means of a gas engine as by the use of boilers and a steam engine.

CHAPTER IV

THE MANUFACTURE OF WROUGHT IRON

Puddling.—Wrought iron is produced from pig iron or east iron by the process of puddling, which is performed in a "reverberatory" furnace. By this process the impurities contained in the iron are almost entirely removed.

The change that has to be made in the composition of pig iron is shown by comparing the composition of Cleveland pig iron, given in the table on page 19, with an analysis of good wrought iron.

Component P	arts.		Cleveland Pig Iron.	Wrought Iron Produced.
Phosphorus Graphitic carbon Combined carbon Silicon Sulphur Mangoliese Slag Iro			1.60 3.20 0.50 2.60 0.08 0.60	0·16 0·04 0·25 0·03 0·01 2·66 96·85
		-	100.00	100.00

A purer wrought iron than that shown by the above analysis may be obtained if required.

The change in the composition is effected by the "oxidation of the impurities. That is, the pig iron is heated to a high temperature so that the oxygen in the air and in the lining of the furnace shall chemically combine with the impurities and separate them from the iron.

The puddling process consists of melting pig iron in a furnace and stirring, or, as it is called, "rabbling" it, so as to bring the whole of the molten metal into contact with the lining of the furnace.

The furnace is lined, bottom and sides, with a material which is called the "fettling." The fettling is composed chiefly of oxides of iron, which, when heated, give up their oxygen.

The oxygen combines with the impurities (carbon, silicon, manganese, phosphorus, and sulphur) in the pig iron, and the solid chemical compounds thus formed enter into the slag.

The gas CO₂, made by the oxidation of the carbon, escapes to the chimney. As oxygen is given off, metallic iron is melted away from the fettling; some of it mixes with the molten pig iron and some goes into the slag. The iron in the charge is thus increased in quantity, and the fettling diminishes; the latter has to be continually renewed.

Oxidation is further assisted by an oxide of iron which is put in with the charge of pig iron, and also by the oxygen contained in the air which enters the furnace.

Fig. 1s a sketch of a puddling furnace.

Bituminous coal is burnt in a grate at one end, and the flame from it strikes against and heats the sloping

24 THE MANUFACTURE OF IRON AND STEEL

roof at the other end. Heat is "reflected," from the roof, and the flame is "beaten back" by the roof on to the pig iron.

This type of furnace is called a reverberatory furnace.

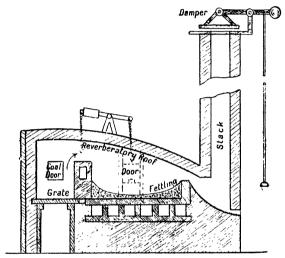


FIG. PUDDLING FURNACE

The word "reverberatory" means "beaten back." The fuel does not come into contact with the pig iron.

FETTLING

Son e materials used for fettling are :-

Best tap.—The cinder or slag from reheating furnaces which are worked with basic bottoms.

Bull dog.—The einder or slag from a probling furnace which has been roasted in a reheating furnace to render it less fusible.

Purple ore, hematite ore, and pottery mine are also used for fetting.

The following table is an analysis of best tap and bull dog:—

Components.	Chemical Formula.	Best Tap.	Bull Dog.
Ferrous oxide	$ \begin{array}{ c c c } \hline & FeO \\ Fe_2O_3 & \\ MnO & \\ SiO_2 & \\ P_2O_5 & \\ \end{array} $	62·0 27·0 1·2 8·0 1·0	4·0 70 0 0·6 24·0 0·7
Sulphur Lime	CaO MgO	0:5	0.7
		99.7	100.0

The tops of the iron bed-plates are covered with best tap to a depth of 3 inches. The furnace is then heated sufficiently to cause the best tap to soften, and it is then covered with a 2-inch layer of bull dog or some other kind of fettling. The kind of fettling is selected according to the quality of the pig iron and the quality of the wrought iron which is required to be produced.

Some scrap iron is now thrown into the furnace and raised to a welding heat; it becomes oxidised, and, by means of an iron tool, is pushed about the furnace in order to oxidise the surface of the fettling.

The furnace is now ready for puddling, and pig fron, together with some "hammer scale," is thrown in. The black flakes of ferrous oxide which fall off wrought iron or steel when it is being forged are called hammer scale. During the melting of the pig iron, silicon,

manganese, and some of the phosphorus are oxidised; these elements leave the pig iron and combine with some of the melted fettling to form the slag. To quicken oxidation, the molten metal is rabbled with an iron tool called a "rabble."

The carbon and most of the remaining phosphorus is now oxidised. CO gas escaping through the molten iron to the surface gives it the appearance of boiling. The CO gas burns with a blue flame, and, taking up more oxygen from the air, passes away as CO₂.

Some slag is now tapped off. Then the temperature of the furnace is reduced so that the iron may become in a pasty condition; that is, not quite fluid. The iron is separated into masses of about 100 lbs. each, rolled into balls, removed from the furnace and hammered under the steam hammer. Hammering expels most of the slag, but not all of it. The balls are shaped into rough oblong blocks called "blooms," and are then taken to the forge rolls to be rolled into bars of different shapes—rounds, squares, and flats. If large blooms are required, two balls are welded together under the steam hammer.



CHAPTER V

THE MANUFACTURE OF STEEL

Steel is a compound of iron and carbon; other elements in small percentages only may be contained in it. The difference between cast iron, wrought iron, and steel depends chiefly on the relative amounts of carbon in chemical combination with the iron. The usual percentages of carbon are:—

					3.25
				.	3.25
				.	0.04
	ites an	d brie	dges		0.15 to 0.2
					0.2 to 0.25
~					0.3 to 0.4
					0.7
				. !	1.0
					1.2
					1.5
	boiler 1	boiler plates	boiler plates .	boiler plates	boiler plates

If steel contains 0.5 per cent. carbon and 1 per cent. sulphur it is red short; if it contain more than 1 per cent. phosphorus, it is cold short. 0.03 per cent. of phosphorus renders steel useless for cutting tool.

Manganese considerably mitigates the ill effects of sulphur and phosphorus. If manganese is present in steel, and if the steel is low in carbon, 0.1 per cent. of phosphorus is permissible for some purposes. Good rails may be made of steel containing 1 per cent. manganese and 0.1 per. cent. phosphorus.

Blister steel.—Blister steel is made from long flat bars, about 3 inches wide and $\frac{3}{4}$ -inch thick, of the purest wrought iron. The wrought iron is converted into steel by *cementation*, by which process carbon is added to the bars.

Fig. 7 shows a transverse section of cementation The firegrate extends from the front to the back, and two cementation boxes are placed above, one on each side of the grate. The inner walls and arch are built of firebricks. The cementation boxes, usually about 15 feet long, 4 feet wide, and 3 feet deep, are made of fire-stone slabs cemented together with fireclay. The boxes are packed with alternate layers of charcoal and flat bars; the top and bottom layers are of charcoal. All the bars must have both sides in contact with the charcoal. The top layer of charcoal is covered with "wheelswarf" to prevent access of air to the iron bars. Wheelswarf is collected from the troughs of grindstones. When a tool is ground on a grindstone, steel dust from the tool mixes with he silica dust which is worn away from the The heat of grinding causes some of the steel to become oxidised; so wheelswarf is a mixture of steel, oxide of iron, and silica. Wheelswarf melts slightly when the furnace is in operation, and it forms n airtight cover. The cementation boxes must be absolutely airtight. A fire is maintained in the firegrate so as to keep the bars heated to a bright orange colour from six to nine days, according to the quality of the wrought iron and to the quality of the steel which is required to be produced.

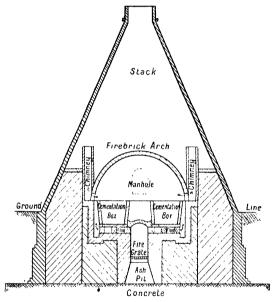


FIG 7 CEMENTATION FURNACE

The effect of the process is to cause carbon from the charcoal to penetrate into the iron bars; this is alled "carburisation" of the iron.

When the bars are being packed, a few bars are placed with their ends protruding through slots at one end of the boxes. A bar can be drawn out through the slot, and the slot is then closed up with fireclay.

When the bar is cold, it is broken and the fractive examined to see if carburisation has proceeded far enough; allowance being made for further carburisation of the bars remaining in the boxes during the time of the cooling of the furnace.

The bars were originally fibrous and tough; when taken from the boxes they are brittle and covered with blisters. Hence the name, "blister steel." When broken, the fracture is of a crystal appearance and shows no fibre. The bars nearest to the firegrate are more highly carburised than the others. None of the bars is carburised right through to the centre, so the centre still remains as iron. If air gains access to the bars during carburisation or cooling, the surface becomes oxidised; such bars are known as "aired bars."

Single shear steel is produced by welding together six bars of blister steel and rolling them out to the required shape. This makes a fairly uniform mixture of iron and steel.

Double shear steel is produced by welding and rolling together two bars of single shear steel; the iron and steel are then more intimately mixed. When the bars are raised to a welding heat, they must be protected to prevent a loss of carbon. They are covered with gypsum (calcic sulphate, CaSO₄), which melts in the fyrnace and forms a coating on the bars.

CRUCIBLE CAST STEEL

Blister steel contains some slag, and the arbon is not evenly distributed throughout its mass. To obtain a homogeneous steel it is necessary to melt the blister stace. Wrought-iron bars may be converted into steel in the crucible by an addition of charcoal or an alloy of iron and carbon; but the best qualities of crucible cast steel are made from blister steel. The bars of blister steel are broken into small pieces and melted in a small crucible made of a mixture of different kinds of

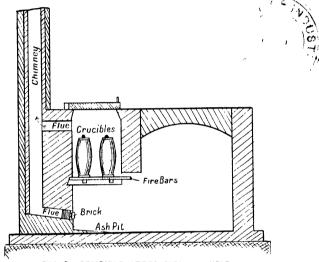


FIG 8. CRUCIBLE STEEL MELTING HOLE

fireclay. The crucible stands on a disc of fireclay and has a lid of the same material.

A section of a steel melting hole is shown in fig. 8. Each hole contains two crucibles which are heated in the furnace by coke fuel packed all round them. The temperature of the furnace is regulated by means of a brick placed in the flue at the bottom of the stack. When the brick stops up the flue, a draught of air passes up between the fire bars and through the furnace to the

stack. The draught is caused by the air being heated when passing through the glowing coke. If the brick is removed, cold air rushes through the flue to the stack, and the draught is lessened. With less draught the coke burns more slowly and less heat is given forth.

A compound containing manganese is charged into the crucible with the blister steel. When the steel is in the right condition to be removed from the furnace, the crucibles are lifted with tongs, the slag is skimmed off, and the contents poured or "teemed" into moulds. The moulds are of cast iron, each in two halves held together by rings and wedges. The steel may be prevented from adhering to the moulds by previously exposing the inner surfaces of the moulds to the smoky flame of burning coal tar, thus covering the surfaces with a fine deposit of soot.

Considerable experience is necessary in order to be able to judge correctly the temperature at which to teem the molten steel. Steel which is low in carbon requires to be teemed at a high temperature, but as soon as possible after it has become fluid. Steel selected with more carbon than is required in the finished steel requires "killing" or "dead melting"—that is, it is kept in the furnace for some time after it has become fluid, until it has quieted. It should not have any ebullition after it is teemed, or the ingot will be honeycombed (porous).

The steel in the fluid state contains a large quantity of gases; such gases are called occluded gases. The greater proportion of these gases should be separated whilst the crucible is in the furnace, instead of after the

steel is teemed. If a large quantity of gases separate during solidification, the steel will be porous.

The equieting is effected by the reaction upon the carbon of the iron oxide contained throughout the mass of molten metal; CO gas is formed and escapes. Part of the oxide of iron is reduced and part floats to the surface of the metal. When the evolution of gases ceases, the metal is quiet.

If kept too long in the furnace, the steel will be brittle on account of its having taken up too much silicon from the crucible.

The very small percentages of phosphorus and sulphur contained in wrought-iron bars made from the best Swedish pig iron, are not injurious, but the steel unavoidably receives a slight addition of sulphur which is given off from the coke and penetrates through the crucible. The steel, however, takes up some manganese from the compound of manganese charged into the crucible, and this destroys the ill effects of the sulphur.

Ferro-manganese is the compound generally used, the chemical action of which is shown by the following equation:—

FeO + Mn = Fe +
Ferrous oxide and manganese yield iron and
MnO.
oxide of manganese.

The oxide of iron rises to the surface of the metal and combines with the silica of the crucible to form manganese silicate. During killing or dead melting, the manganese silicate is acted on by the excess carbon in the steel, and silicon is set free.

34 THE MANUFACTURE OF IRON AND STEEL

 2MnO,SiO_2 + C = Si + Silicate of manganese and carbon yield silicon and CO_2 + 2MnO. - carbon dioxide and oxide of manganese.

The silicon enters into the steel and hastens the liberation of the CO₂ gas; so it assists in quieting the metal. A percentage of 0.02 of silicon will not be injurious, but the steel is liable to take up more than this amount during killing. The addition of 0.03 per cent. of aluminium just before teeming has the same effect as silicon in quieting the metal.

The chemical action of the oxide of manganese with the silica of the crucible at the surface of the metal cuts a groove in the crucible, so the charge has to be reduced for the next melting. The first charge is about 60 lbs.; the second 54 lbs.; and the third 48 lbs. These three charges are completed in one day, and a new crucible is required for the next day's work.

MILD STEEL

Mild steel is not as pure a steel as tool steel, but it is more suitable for most purposes for which steel is used. Mild steel is crystalline and free from slag; wrought iron is fibrous and contains slag irregularly mixed with it. Mild steel is now much more generally used than wrought iron, because:—it can be preduced in larger masses, is more uniform in composition throughout its mass, has a greater tensile strength, and is cheaper to produce. Wrought iron, however, has the advantage that, owing to its fibrous composition, of it can endure a great deal of hammering during forging

without deterioration. It may also be reheated very many times.

Component Parts.					Mild Steel.	Good Wrought
						Iron.
Phosphorus				.	0.05	0.16
Carbon .				.	0.20	0.04
Silicon .					0.02	0.25
Manganese				.	0.50	0.01
slag .					None	2.60
iron				- ;	99.18	96.85

The Siemens-Martin process for the manufacture of steel consists in melting pig iron, or pig iron together with scrap steel or iron, in an "open-hearth" furnace. The silicon and manganese are oxidised. Hematite ore is added to the molten metal, and the oxygen contained in it will oxidise the carbon. The metal in the furnace is then nearly pure iron, and it is converted into medium or hard steel by the addition of spiegeleisen in the furnace. Steel is then tapped from the furnace.

The iron is converted into mild steel by the addition of ferro-manganese in the furnace, or in the ladle, after the iron has been tapped from the furnace. The Bessemer process consists in oxidising the impurities in the iron by blowing air through fluid pig iron which has been made to flow into a "converter," and then converting it into steel by the addition of spiegeleisen or ferro-manganese.

The Siemens-Martin process is slower, but it is more completely under control than that of the Bessemer, and any grade of steel can be made with more regularity and certainty than by the Bessemer process.

ACIDS AND BASES

The following is a list of some acids and bases which can enter into chemical union with each other so that the resulting compound has a much lower melting-point than either the acid alone or the base alone.

Acids.	Chemical Formula.	Bases.	Chemical Formula.
Phosphoric acid . Titanic acid . Silica Carbon dioxide, or } carbonic acid	$\begin{array}{c} P_2O_5 \\ TiO_2 \\ SiO_2 \end{array}$	Ferrous oxide Manganous oxide . Lime Magnesia .	Fe() Mn() CaO MgO

The union of the "acid" silica with the "base" lime in the blast furnace is an example.

Alumina (Al₂O₃) acts as an acid when lime predominates and as a base when 'silica is the chief component.

Acid steel.—The Siemens furnace and the Bessemer converter were formerly lined only with material which consisted chiefly of silica.

Silica is an acid, so is phosphoric acid; therefore silica will not assist in eliminating phosphorus from iron.

Only pig iron which contains a small percentage of phosphorus can be converted into good steel by the acid process.

**Basic steel.—Most iron ores contain a considerable amount of phosphorus, and, as has already been stated, it all goes into the pig iron during smelting. Thus it was necessary to discover some means of eliminating the phosphorus. The discovery of the "basic" process, by which phosphorus and sulphur can be eliminated from some kinds of pig iron, has greatly increased the production of mild steel; as pig iron, formerly useless for steel-making, is now being converted into steel.

CHAPTER VI

THE SIEMENS-MARTIN OR OPEN-HEARTH PROCESS

THE heat in the open-hearth furnace is obtained by the combustion of "producer" gas.

GAS PRODUCER

Small coal is burnt in a producer and converted into gases which can be collected and conveyed to the furnace where they are required to be burnt. The gases generated are carbon monoxide (CO), methane or marsh gas (CH₄), and hydrogen (H); these are all combustible.

A gas producer is shown in fig. 9. It is built of firebricks with an outer covering of steel plates. The whole structure is set on pillars over a recess which contains water.

A fire is first lighted at the bottom, and coal is charged into a "hopper" at the top. Fuel is admitted to the producer from the hopper by means of a cup and cone arrangement, as in a blast furnace. The necessary air, generally preheated, for combustion is forced in by injecting steam into a pipe with an enlarged entrance. It enters the producer through a steam and air flue and escapes from under a central cone. The central cone

helds up the fuel until it is consumed; the ashes drop into the water and are raked out. The gases ascend and are led away by the downtake. Ammonia can be extracted from the gases before they are led away to the furnace to be burnt.

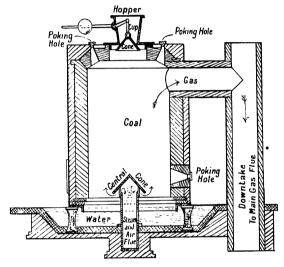


FIG.9. GAS PRODUCER

THE OPEN-HEARTH FURNACE

Fig. 10 is a ventical longitudinal section of an openhearth furnace worked on the regenerative system. The whole is built of firebrick and strengthened by steel plates and old rails braced together by tie rods. The furnace is built over four arches which are the arches of the regenerators, one on each side for gas and one on each side for air. The regenerators are filled with checkered bricks in the same way as in the regenerator

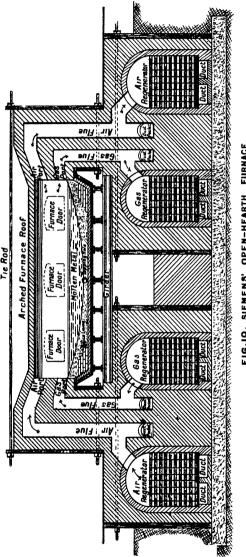


FIG.10. SIEMENS' OPEN-HEARTH FURNACE

of ... hot-blast stove (see page 13). The outer ones are for air and the inner ones are for gas, but it may be arranged that the outer ones are for gas and the inner ones for air.

The gases and air are led from the regenerators by flues to ports in the inner walls of the furnace. There may be one gas and two air ports at each end of the furnace, or two gas and three air ports. The air ports are at a higher level than the gas ports.

The "dust pockets" are for the purpose of collecting the dust (and sometimes slag) blown out of the furnace. If the dust was allowed to go into the regenerators, they would become choked.

When the furnace is at work, the gases from the producer are led through a "duct" in the ground to the bottom of the gas regenerator, and through the regenerator to the gas port, or ports, in the furnace.

Air passes through another duct in the ground to the bottom of the air regenerator, and thence to its ports in the furnace.

The ducts, flues, and ports for the gases are quite separate from the ducts, flues, and ports for the air, but they are built in exactly the same way on each side of the furnace. The gases and air meet and are ignited in the furnace. As the ports are built with a slope inwards, the flame is directed on to the metal in the furnace.

The products of combustion pass out through the opposite ports at a very high temperature and heat the regenerators on the other side on their way to the chimney.

The arrows in the figure indicate the directions of the

gases and air entering the regenerators on the left de and leaving the regenerators on the right side. When the gases and air have travelled in this direction for a certain length of time, say twenty minutes, the regenerators on the right side will have become greatly heated; the gas and air valves are then reversed so as to cause the gases and air to enter the furnace through the opposite ports and in the opposite direction. That is, the gases and air will be made to pass upwards through the regenerators on the right side. The gases and air will be heated by passing between the very hot bricks, and when they ignite in the furnace the flame produced will give a more intense heat than before. In the meantime, the regenerators on the left side are being heated by the outgoing gases.

The valves are at intervals reversed, so that the gas and air regenerators on one side and the gas and air regenerators on the other side are alternately heated and cooled. With each reversal the furnace becomes more highly heated until a temperature is attained which melts the iron.

The roof of the furnace becomes greatly heated and reflects its heat on to the metal. The bricks of the roof are built with an arch to prevent them from falling in.

As the whole structure expands on being heated, the nuts at the ends of the tie rods are gradually screwed back. When steel-making is finished, the furnace is allowed to cool down gradually, and as it cools, the nuts on the tie rods are screwed up. The bottom of the furnace consists of firebricks on steel plates supported by girders.

LINING THE FURNACE FOR THE ACID PROCESS

The furnace is lined with white or silver sand mixed with a small quantity of ganister. The former is found chiefly in Belgium; it is almost pure silica (silica, $98\frac{1}{2}$ per cent.) and is infusible at the furnace temperature. Ganister is found in large quantities near Sheffield; it contains a less percentage of silica (silica, $94\frac{1}{2}$ per cent.) than white sand, and the other materials contained in it are fusible at the furnace temperature, so it acts as a binding material.

A thin layer of the mixture is laid over the bottom firebricks, and when the heat of the furnace is sufficient, it "frits" (melts slightly) and adheres to the bricks. The mixture is continually added in thin layers until the bottom of the furnace has a thick lining of sand. The grains of sand frit just sufficiently to stick to each other.

Some acid slag is then thrown into the furnace and melted and rabbled over the furnace bottom so as to glaze the surface of the sand. The slag is tapped off.

Charging the furnace.—The furnace is charged with a small quantity of pig iron and, on top of the pig iron, scrap steel or iron. Light scrap should be kept off the bottom and clear of the banks of the furnace, as it quickly oxidises and would cut grooves in the silica lining.

The furnace is not charged to its full capacity until it has been worked for three or four days; it should be kept in continual operation, day and night, until repairs are necessary. A furnace is usually worked continuously for two and a half to three months.

44 THE MANUFACTURE OF IRON AND STEEL

If there is a large quantity of scrap steel to be disposed of, a charge for a 15-ton furnace may be:—8 tons of pig iron, 5 tons of scrap steel, $1\frac{1}{2}$ tons of hematite ore as the oxidising agent, and $2\frac{1}{2}$ cwts. of ferromanganese at the end of the process to convert the iron into steel.

CHEMICAL ACTIONS IN THE ACID OPEN-HEARTH PROCESS

Good acid open-hearth steel may be manufactured from pig iron containing the following elements:—

Element.			Pe	rcentage
Carbon				3.2
Silicon				2.0
Phosphorus	•			0.02
Sulphur	•			0.02
Manganese				0.75

In the acid process neither phosphorus nor sulphur is eliminated. In fact, the percentages are greater in the finished steel than in the original pig iron, as the iron when molten absorbs slight amounts of phosphorus and sulphur from the hematite ore and from the spiegeleisen or ferro-manganese. So phosphorus and sulphur should not be contained in the pig iron in a greater proportion than 0.05 per cent.

The eliminations of the impurities in the charge take place in three stages:—

- 1. During melting, by the oxidising action of the flames.
- 2. After melting, by the action of the oxides of iron, formed during melting.

3. During boiling, by the action of the oxide of iron added to the charge.

In the first stage, "during melting," about one-half of the silicon and one-third of the manganese are oxidised.

In the second stage, "after melting," nearly all the remaining silicon and manganese are eliminated and the carbon has been diminished. The oxidised products, silica (SiO₂), oxide of manganese (MnO), and some oxides of iron (FeO and Fe₂O₃) go into the slag.

At this point a hematite ore containing 70 to 80 per cent. of ferric oxide is charged, in small quantities at a time, into the furnace.

In the third stage, "during boiling," nearly all the carbon is oxidised; the escape of CO gas through the metal gives the appearance of boiling. If the hematite ore is added too quickly, the ebullition may cause some metal to run out of the furnace doors. The ferric oxide in the ore is decomposed, and its oxygen quickens the burning out of the carbon; the iron which separates from it adds to the molten metal in the charge.

The chemical equation is :--

 $3C + Fe_2O_3 = 2Fe + Carbon$ and ferric oxide yield iron and 3CO.

carbon monoxide.

The gas CO burns at the surface of the metal, and taking up more oxygen from the air, it escapes as CO₂.

Before finishing, it is beneficial to place a few half-

pigs of hematite iron, containing much carbon and silicon, just inside the doors of the furnace. When they are red-hot, push them into the melted metal and rabble quickly; this will deoxidise the charge and make it quiet for tapping.

If medium or hard steel is required, a certain weighed quantity of spiegeleisen is now thrown into the furnace and the charge is almost immediately tapped.

If a mild steel is required, the iron is tapped from the furnace, and ferro-manganese is thrown into the ladle at the same time as the metal flows in, or it may be added to the charge in the furnace before tapping.

The approximate compositions of spiegeleisen and ferro-manganese are as follows:—

ment	ts.		Spiegeleisen.	Ferro-magganese.
			5·00 15·00 0·80 0 02	6:30 77:00 0:80 0:01
		:	0·10 79·08	0·10 15·79

Before tapping, samples should be taken out in an iron spoon, cooled, hammered flat, and broken. The appearance of the fracture will indicate the qualities of the steel; the percentage of carbon may be judged approximately.

To ascertain the percentage of carbon exactly, the sample is submitted to a chemical colour test. The test is made as follows:—

Fine drillings are taken from the sample—we will call these drillings "sample A"—of exactly equal weight to another sample which we know to contain the percentage of carbon which we require in our charge in the furnace. The latter sample we will call "sample B."

Samples A and B are placed separately into two similar test tubes, and into each tube is poured an equal quantity—by measurement in a glass tube—of colourless nitric acid. The nitric acid dissolves the samples of steel. The steel will be dissolved more quickly if the test tubes are heated by lowering them into a vessel containing boiling water.

When it is seen that the steel is all dissolved, the colours of the solutions in the test tubes are compared. The colours vary from a light straw to a dark brown. If the solution in which sample A is dissolved is darker in colour than the solution of sample B, it contains a higher percentage of carbon; in which case it will be necessary to reduce the amount of carbon in the charge by charging more hematite into the furnace.

If, on the other hand, solution A is lighter in colour than solution B, it contains a lower percentage of carbon. The percentage of carbon in the charge must then be increased by adding spiegel or ferro.

The following table is for the purpose of showing approximately the chemical changes that take place during the process:—

			Compositio	on.	
Components.	Pig Iron and Scrap Steel.	When Melted.	At the Commence- ment of Boiling.	Before Ferro- Manganese is Charged.	Finished Mild Steel.
Phosphorus . Carbon . Silicon .	0·05 2·90 1·60	0.05 2.70 0.90	0.051 2.500 0.400	0 051 0·100 0·020	0.052 0.190 0.020
Manganese . Iron	0·70 94·70	0·50 95·80	0·100 96·89 6	None 99:776	0·550 99·134
	99-95	99-95	99-947	99-947	99-946

The addition of spiegeleisen or ferro-manganese has three effects:—

1. It deoxidises the molten metal. This is shown by the equation:—

The manganous oxide goes into the slag.

- 2. It adds carbon to convert the iron into steel of the required quality.
- 3. It adds manganese to the steel; this to some extent destroys the ill effects caused by the presence of phosphorus and sulphur.

The reason why spiegeleisen is added for medium and hard steels, and ferro-manganese for mild, is made

clear by referring to the table (p. 46) of the compositions of spiegel and ferro.

500 lbs. of spiegel contains 75 lbs. of manganese and 25 lbs. of carbon.

100 lbs. of ferro contains 77 lbs. of manganese and 6.3 lbs. of carbon.

To get the same quantity (75 to 77 lbs.) of manganese in each case, 500 lbs. of spiegel to 100 lbs. of ferro would have to be charged. But 500 lbs. of spiegel contains 25 lbs. of carbon; therefore it will make a harder steel than 100 lbs. of ferro, which contains 6:3 lbs. only of carbon.

Slag.—The following gives an idea of what may be the composition of the slag which results from the process:—

Components	Percentage.	
Ferrous oxide .		26
Manganous oxide		8
Silica .		57
Lime .		6
Alumina, etc		3

The weight of the slag will be about 13 per cent. of the total weight of the pig iron, scrap, and hematite ore charged into the furnace.

=Although the slag contains about 20 per cent. of iron and 6 per cent. of manganese, it does not pay to extract these metals, so the slag is useful only for such purposes as road-making and kallast for railways.

CHAPTER VII

THE BASIC OPEN-HEARTH PROCESS

Many kinds of pig iron contain a medium quantity of phosphorus, too much for it to be used for steel-making by the Siemens acid process, and not enough to enable the necessary high temperature to be maintained in the Bessemer basic process. Such iron can be converted into steel by the open-hearth basic process only.

Basic lining.—The lining of the furnace is the only matter in which the plant for the basic process differs from that of the acid process. The furnace requires a basic lining, so that the base (usually lime) which is added to the charge of pig iron shall not enter into chemical union with it, but shall remain free to combine with the phosphorus as it is oxidised from the pig iron, and to retain the phosphorus in the slag until the process is finished.

Basic materials.—The following table gives the chief components of some basic materials after they have undergone the process of calcination to remove CO₂ and other volatile matters contained in the quarried lumps:—

Compor	onta	Formulæ.		Percentages	
Сотрог	ients.	rormmæ.	Dolomite.	Magnesite.	Limestone.
Lime . Magnesia Silica . Alumina		Ca() MgO SiO Al()	60 32 3·5 3	$ \begin{array}{c} 2 \\ 93 \\ 1 \\ 3 \end{array} $	93 3 2 1

The basic material to be selected depends on which material is the most economical to use in the district in which steel is to be made.

Dolomite is considered the best; it is ground into powder and mixed with about 8 per cent. of anhydrous tar. "Anhydrous" means "without water."

Magnesite is a good material, but expensive in most places.

Limestone mixed with tar is fairly good.

E sic bricks are made from basic materials in a special hydraulic press with moulding boxes; they are then dried in a kiln.

LINING THE FURNACE

The basic material may be spread in thin layers and heated so that it frits together, in the same manner as the silica lining is spread in the open-hearth furnace for the acid process: or the furnace may be lined with basic bricks cemented together with basic material, and covered with the same material.

The former method is the better, as it makes a more solid lining.

. 52 THE MANUFACTURE OF IRON AND STEEL

Basic material is very friable, and therefore it cannot be used for building the walls and roof of the furnace; these are built of silica bricks.

Chemical action is liable to take place between the silica bricks and the basic material; the action is considerably less if the acid and basic materials are not subject to *pressure* in contact with each other.

A method of partly relieving the basic material from

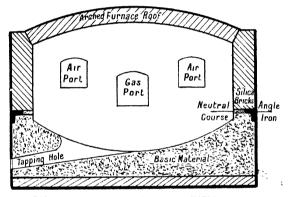


FIG.II. FURNACE LINING. BASIC MATERIAL.

the weight of the walls and roof is shown in fig. 11. An angle iron is riveted on to the inside of the steel plates which form the furnace casing. Chemical action is further prevented by making a joint, which is called a neutral course, between the acid and basic materials. The neutral course is generally a mixture of crushed chrome iron ore and a little tar.

The iron plates at the bottom of the furnace are covered with silica bricks, and the basic material is fritted on to the bricks. When the furnace is in operation, there will be no chemical action between the

bottom silica bricks and the basic lining, as sufficient heat will not penetrate the upper lining.

Charging the furnace.—The pig iron for use in the process should not vary much from the following composition:—Phosphorus, 1.75 per cent.; silicon, not more than 1 per cent.; sulphur, not more than 0.06 per cent.; manganese, 1.75 per cent.; and carbon, 3.5 per cent. 25 to 30 per cent. of scrap, wrought iron, or steel, may be charged with the pig iron. When the charge is melted, lime and an oxide of iron is thrown into the furnace. The oxide of iron may be any form of ferrous or ferric oxide, which contains little or no silica. Best tap, the composition of which is given on page 25, is used, or "pottery mine," which is an iron ore mined in Staffordshire, England.

THE CHEMISTRY OF THE PROCESS

The oxide of iron is the oxidising agent.

Oxilation of silicon:-

$$Si + O_2 = SiO_2$$
.
Silicon and oxygen yield silica.

Silica, which is an acid, is prevented from entering into combination with the basic lining of the furnace by the highly heated lime, which is a base. The silica at once combines with the lime and forms silicate of lime in the slag.

$$2\text{CaO} + {}^{\bullet}\text{SiO}_2 = 2\text{CaO}, \text{SiO}_2.$$
 Lime and silica yield silicate of lime.

Oxidation of carbon :-

$$2C + O = 2CO.$$

· Carbon and oxygen yield carbon monoxide.

The CO gas escapes through the molten metal and gives it a motion with the appearance of boiling. When the CO reaches the surface of the metal, it takes up more oxygen from the air and escapes as CO₂.

Oxidation of manganese:-

$$Mn + O = MnO.$$

Manganese and oxygen yield manganous oxide.

The manganous oxide, which is a base, enters into the slag; it is useful in the process, as it helps to keep the slag more basic than acid.

Oxidation of phosphorus:—

$$2P + 5O = P_2O_5.$$

Phosphorus and oxygen yield phosphoric acid.

The phosphoric acid combines with the lime and remains in the slag as tetra-calcic-phosphate (phosphate of lime).

$$P_2O_5 + 4CaO = 4CaO, P_2O_5.$$

Phosphoric acid and lime yield phosphate of lime.

Silicon and manganese are the first to be completely removed from the pig iron; carbon and phosphorus oxidise more slowly.

Small quantities of lime are added from time to time; too much lime will cause a pasty slag which will be difficult to tap from the furnace. The carbon should not be removed before the phosphorus, as the CO gas on escaping causes a commotion in the metal. This commotion is necessary in order to bring the phosphorus in the metal into intimate contact with the oxide and with the lime. Insufficient lime will cause a charge to go "off the boil," CO ceasing to escape, before enough phosphorus has been eliminated. In this case more

lime is added, and some hot pig iron is charged in order to get the metal again "on the boil."

Samples are taken from the furnace at intervals, and when these are cooled and broken, it can be seen by the appearance of the fracture to what extent the phosphorus has been eliminated.

At the end of the process the slag should be as non-oxidising as possible, as, if too much oxygen is present, the metal cannot be quietly teemed.

The elimination of much sulphur cannot be relied upon, and for this reason a pig iron with a small percentage of sulphur should be selected.

Manganese, during the process, has some slight effect in eliminating sulphur, and when the spiegeleisen or ferro-manganese is added, there is a further small reduction of sulphur.

To convert the iron into steel, spiegel or ferro is added as in the Siemens acid process.

It is not intended that the basic material with which the furface is lined shall be used as a base to absorb the acids, silica, and phosphoric acid—lime is added to prevent that; but the lining becomes gradually worn and damaged, and new layers of basic material are occasionally required.

Slag.—The slag resulting from the process will be approximately of the following composition:—

Component	Percentages.	
-	1	
Phosphoric acid	. !	13
Manganous oxide	.	10
Magnesia		6
Lime		41
Oxide of non .		17
Silica	. i	13

The slag is broken and ground into a fine powder for manure.

If it contains much less lime, or much more silica or oxide of iron than shown in the above composition, it is dense and hard and difficult to break up into small enough pieces for grinding.

The phosphoric acid and lime, especially the phosphoric acid, makes the slag valuable in some soils as a fertiliser.

THE ACID AND BASIC OPEN-HEARTH PROCESSES COMPARED

The chief points of difference between the acid and basic open-hearth processes may now be summarised:—

Aeid.	Basic.
Furnace lined with acid material, chiefly silica.	Furnace lined with basic material.
Hematite pig iron used, Scrap used must contain a small percentage only of phosphorus.	Phosphoric pig iron used.
Hematite ore used as the oxidising agent.	Ore containing phosphorus may be used, but it must contain very little silica.
No elimination of phosphorus. Slag useless as a fertiliser.	Phosphorus is eliminated. Slag valuable as a fertiliser.

As a greater quantity of slag is produced in the basic than in the acid process, a smaller quantity of basic than acid steel is produced in furnaces of equal dimensions.

A great disadvantage of the basic process is that good high earbon steel cannot be made by it. The reason

for this is that a small percentage of phosphorus always passes back from the slag into the metal when ferro or spiegel is added, owing to the reducing action of the carbon and of the manganese.

High carbon steel may be made by recarburising the iron after it is tapped by adding molten spiegel in the ladle; or by the "Darby recarburising process," which consists of passing the metal, as it flows from the furnace, through a perforated vessel, into which falls a stream of fine carbon. In these methods the difficulty is to keep the slag from passing into the ladle.

The differences between mild or medium steels produced by the acid or basic open-hearth processes are not generally shown by chemical analysis or by mechanical tests, but under microscopical examination basic steel shows a more defective grain.

Steel produced by the basic open-hearth process is cheaper than that from the acid open-hearth, and it is largely used in America, Germany, and Belgium. But Engish manufacturers consider that while basic steel is suitable for many requirements, it fails entirely, as compared with acid steel, in endurance tests, when used for tyres, angles, forgings, or for spring steel. Even for rails, acid steel is preferred.

Experience has shown that acid steel resists "fatigue" (see Vanadium, page 87) better than basic steel.

CHAPTER VIII

THE ACID BESSEMER PROCESS

The acid Bessemer process is carried out in a vessel which is called a *converter*. The pig iron to be converted into steel must be low in phosphorus and sulphur, and be similar to the composition, given on page 44, of the pig iron used in the acid Siemens process.

Melted pig iron is poured into the converter, and it is purified by blowing a large quantity of air through it; the oxygen contained in the air is the oxidising agent.

Fig. 12 is a section of a Bessemer converter built of steel plates and lined with firebricks and ganister." It is charged and emptied through the one open end; at the other end are the tuyere holes through which the air blast is forced.

The converter is encircled at its widest part by a steel ring, to which two trunnions are secured. The trunnions rest on bearings and act as axles. One axle is a tube through which the air blast passes to the bottom of the converter

A toothed wheel, in gear with a pinion, is secured to the axle; as the toothed wheel is revolved, it rotates the converter to any required position. The converter is made up of three parts which are bolted together. The three parts are called the hood or nose, the body, and the bottom or plug.

LINING THE BESSEMER CONVERTER

Ganister, which is found near Sheffield, England, and other places, is the material used for lining the converter; it consists chiefly of silica, but has other more casil; fusible materials contained in it, which enables the whole to bind firmly together.

The three parts of the converter are lined separately. The hood is inverted and a wooden core is placed within it; the space between the core and the hood is filled and rammed with ganister. The bottom is also rammed with ganister, openings being left for the insertion of the tuyeres. The body is lined with silica bricks cemented with ganister.

The tuyeres are tapered plugs which have been moulded out of fireclay; they are cemented into the openings in the bottom of the converter with fireclay or ganister, and are held in position by means of a steel plate. Each tuyere has from 12 to 20 holes about $\frac{5}{10}$ -inch in diameter.

Owing to the violence of the air blast, the bottom lining has to be frequently repaired—generally after about 20 "blows." The hood and body may not need relining more often than once a year.

CHARGING AND WORKING THE CONVERTER

A fire is lighted in the converter to heat it before charging with metal. The metal may be pig iron melted in an ordinary foundry cupola.

60 THE MANUFACTURE OF IRON AND STEEL

In this way the pig iron may be selected of a uniform quality, and the steel manufactured from it will also be uniform in quality.

It is, however, much more economical in fuel and labour to charge the converter with molten metal direct from the blast furnace.

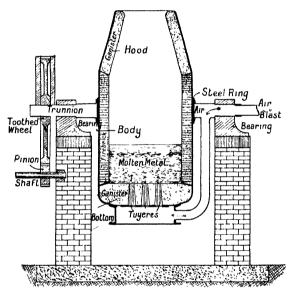


FIG.12. BESSEMER CONVERTER

If the metal is taken from a single-blast furnace, it may vary in quality, as blast furnaces often produce irregular qualities of iron.

It is, therefore, usual to tap iron from several blast furnaces into a large vessel which is called a *mixer*.

One or two furnaces may produce iron high in silicon or sulphur, and this may be compensated for by iron from other furnaces being low in silicon or sulphur. The iron obtained by mixing the tappings of four or more blast furnaces is of a fairly uniform composition.

The mixer is a large tipping ladle—that is, a ladle which is emptied by rotating it on its trunnions.

Metal is poured from the mixer into another tipping ladle, which is carried on rails to the converter. As this ladle is being filled, it stands on a weighing machine, so that the actual quantity of molten metal which it

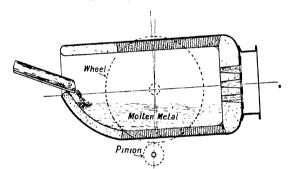


FIG 13 CHARGING THE BESSEMER CONVERTER

contains is known; the quantity is sufficient for one "blow" in the converter.

Before charging the converter with metal, it is rotated to a horizontal position as shown in fig. 13. In this position the metal-cannot flow into the tuyere holes. When the converter is charged, the air blast is started and the converter rotated to a vertical position.

• The pressure of air, 20 to 25 lbs. per square inch, prevents the metal from flowing into the tuyere holes, and the metal is kept in motion by the force of the air. The air passes up through the hot fluid metal,

and, in so doing, the oxygen of the air enters into chemical combination with the silicon, carbon, and manganese.

In some converters the tuyeres are placed on one side and slightly inclined downwards, just above the level of the molten metal when the converter is upright; air is then blown on to the surface of the metal. Such converters are called side-blown or surface-blown converters. The air blast causes a roaring sound, and a long flame issues from the opening at the top of the converter. The flame changes in colour during the continuation of the air blast; first it is violet, then orange, and then a dazzling white. After this the colour becomes of a faint blue and the flame almost disappears—the flame is then said to "drop"; at the same time there is a change in the sound of the blow. This indicates that all the carbon has been oxidised. The oxidation of the silicon and the manganese is completed before the oxidation of the carbon.

The converter is then immediately rotated to a horizontal position and the air blast stopped.

The slag, on account of its being of lower density, separates from the iron and rises to the surface.

The metal is now highly oxidised; it is supposed that at this stage free oxygen or an oxide of iron exists, dissolved with and clinging to the metal. Hot ferromanganese or spiegeleisen is now thrown into the converter, and, as it melts, the iron is deoxidised, receives the required percentage of carbon, and is converted into mild or medium steel.

The steel is now teemed into moulds by further rotating the converter.

CHEMICAL ACTIONS IN THE ACID BESSEMER PROCESS

The following table is an example of the chemical changes that take place during the process:—

Components.	Hematite Pig Iron before Blowing.	Hematite Pig Iron after Blowing.	Mild Steel produced after addition of Ferro-manganese.
Carbon Silicon Phosphorus Sulphur	3·5	None	0·2
	2·0	None	0·02
	0·05	0.053	0·055
	0·05	0.053	0·053
	0·75	Slight trace	0·55

There is no elimination of phosphorus or of sulphur, but as the quantity originally present is now concentrated in a smaller weight of metal, the percentage of each becomes slightly greater.

The chemical reactions in the process are shown by the following equations:—

 $C + O_2 = CO_2.$

Carbon and oxygen yield carbon dioxide.

The gases CO and CO₂ escape into the air.

 $Si + O = SiO_2$. Silicon and oxygen yield silica.

Silica forms the chief component of the slag.

Mn + O = MnO. Manganese and oxygen yield manganous oxide.

The manganous oxide goes into the slag.

64 THE MANUFACTURE OF IRON AND STEEL

A small quantity of iron is oxidised.

Fe + O = FeO. Iron and oxygen yield ferrous oxide. $2\text{Fe} + 3\text{O} = \text{Fe}_2\text{O}_3$. Iron and oxygen yield ferric oxide.

These oxides of iron go into the slag.

When the ferro-manganese or spiegeleisen is added, deoxidisation may be supposed to take place, thus:--

Fe() + Mn = MnO
Ferrous oxide and manganese yield manganous oxide
+ Fe.
and ron.

HEAT MAINTAINED DURING A BESSEMER BLOW

The fluid metal is poured into the converter at a high temperature, and a large quantity of cold air is forced through it. The metal, however, is not reduced in temperature, but it is actually hotter at the end of the blow than at the beginning. The increase in temperature is chiefly due to the burning of the carbon and the silicon. Most of the heat evolved by the oxidation of the carbon is carried away in the gases which escape, but the silica resulting from the oxidation of the silicon remains at a very high temperature in the slag. This slag protects the metal and keeps it in a fluid condition. It is necessary to have a certain percentage of silicon in the pig iron to maintain the heat required for the acid Bessemer process.

If the metal is too hot at the finish of the process, owing to the iron containing too great a percentage of

silicon, it will be in a disturbed condition resembling boiling when poured into the moulds, and the ingots will be unsound.

A remedy for this is to throw some scrap iron or steel into the converter before pouring in the melted pig iron; the heat of the whole mass of fluid metal is thus lessened by heat being absorbed in melting the scrap. With an overhead shoot arrangement, scrap may be thrown into the converter during the blow.

If the metal is too cold at the finish of the process, the ferro-manganese or spiegeleisen does not become properly mixed with the fluid iron; the metal is not sufficiently fluid to pour evenly into the moulds, and some of the steel may solidify in the ladle. In this case, iron containing more silicon should be used; or, if this cannot be obtained, a greater volume of air blast, causing more rapid oxidation, may produce sufficient heat.

Acid Bessemer slag contains about 9 per cent. of iron and 12 per cent. of manganese, but, like acid Siemens slag, the composition of which is given on page 49, it does not pay to extract these metals.

CHAPTER IX

THE BASIC BESSEMER PROCESS

By the basic Bessemer process good mild steel may be made from steel containing much ($2\frac{1}{4}$ to $3\frac{1}{2}$ per cent.) phosphorus.

The plant required is the same as in the acid Bessemer process, the only difference being that the converter is lined with basic material instead of acid material.

The converter for the same amount of steel produced must be of larger dimensions for the basic process than for the acid process, as more slag results from the basic process.

Machinery for grinding the slag into powder is also required.

LINING THE BASIC BESSEMER CONVERTER

Dolomite, the composition of which is given on page 51, mixed with anhydrous tar, is the most generally used basic material.

The hood, which is the least liable to be damaged, is often lined with a mixture of new dolomite and old dolomite ground fine, tar being added to the mixture. The hood is inverted and a wooden core placed within

it; the space between the core and the hood is filled and rammed with basic material. The body is lined with bricks which are made of compressed dolomite and tar, and these are cemented together with dolomite and tar. The bottom or plug is also made of the same materials well rammed. Holes, \(\frac{3}{4}\)-inch diameter, are left in the plug to serve as the tuyere holes for the air blast. About 90 holes would be required for a 20-ton converter.

After the bottom is bolted on, the space between it and the body is filled with basic material.

The mixed dolomite and tar is always rammed with very hot rammers, which are iron bars enlarged at one end, and as the basic material is put on in thin layers, the heat of the rammers causes the layers to become cemented together into a strong solid block.

The plug quickly becomes worn out and the basic material has to be renewed. The plug may perhaps be used for 20 blows, the lining of the body for 100 blows, and the lining of the hood for 200 blows.

CHARGING AND WORKING THE CONVERTER

A quantity of calcined lime, 3 to 4 cwts. per ton of iron, is first thrown into the converter. The converter is then rotated until it is in the position shown in fig. 13, page 61, in which position it receives the charge of molten pig iron from a mixer or cupola.

The air blast is then started and the converter brought back to a vertical position.

The air blast is continued until the flame "drops," and for a short time after.

There is the period 13 to 15 minutes of the blow until the flame drops, and another period 3 to 4 minutes, which is called the "after-blow."

Nearly all the phosphorus is oxidised during the after-blow.

When the after-blow is considered to be sufficient, the converter is rotated to a horizontal position and the air blast stopped.

After allowing a short time for the slag to separate from the iron, a sample of the metal is taken from the converter by means of a long-handled spoon, and this is solidified in an open mould, hammered flat, cooled with water, and broken. By the appearance of the fracture it may be judged whether or not the metal is sufficiently free of phosphorus; if high in phosphorus, long bright crystals will be shown in the fracture.

If the metal contains too much phosphorus, the blow will have to be restarted for a short time and then another sample taken and examined.

If the examination of the sample is satisfactory, as much as possible of the slag is quickly poured off, and the process is finished by the addition of ferromanganese or spiegeleisen to the iron to convert it into steel.

CHEMICAL ACTIONS IN THE BASIC BESSEMER PROCESS'

The following table is an example of the chemical changes that take place during the process:—

•	Composition of			
Components.	Pig Iron charged.	Metal at end of Blow.	Metal at end of After-blow.	Mild Steel after addition of Ferro.
Carbon Silicon Phosphorus . Sulphur Manganese .	3·6 1·0 2·6 0·07 1·2	0·06 0·02 2·3 0 066 0·16	Trace None 0·04 0·055 0·13	0·18 0·02 0·05 0·055 0·6

Lime, which is a base, is used in the process, as it combines with the phosphorus and holds it in the slag. When a sample of molten iron is taken from the converter for examination, it is often considered necessary to add more lime before continuing the after-blow.

The presence of silicon, which is necessary to maintain the heat in the acid Bessemer process, is of disadvantage in the basic Bessemer process, as by combining with the lime it renders the slag less basic, and this retards the elimination of the phosphorus. To get the best results the silicon should not exceed 1 per cent., but basic Bessemer steel may be made from pig iron containing 1.5 to 2 per cent. of silicon. If the percentage of silicon is high, a large quantity of lime will be required, and the melting of the lime takes up much of the heat given by the oxidation of the silicon. It is important that the lime to be used should be as free as possible from silica.

With 1 per cent of silicon the iron should contain about 3 per cent of phosphorus to obtain the heat

necessary in the blow. Great heat is produced by the oxidation of the phosphorus, and, as little is oxidised until the beginning of the after-blow, the greatest heat is obtained during the after-blow. Great heat is necessary for the elimination of the phosphorus and the sulphur. It is desirable to have a larger percentage of manganese in the pig iron for the basic process than for the acid process. It is oxidised from the commencement of the blow, and the heat of oxidation makes up to some extent for the percentage of silicon being low.

As manganous oxide, which is formed by the oxidation of manganese, is a base, less lime is required if there is a large percentage of manganese.

Sulphur is nearly all oxidised during the after-blow, when there is an excess of ferric oxide, a high temperature of metal, and a fluid slag.

If the percentage of sulphur in the pig iron is high, say 0.3 per cent., about 70 per cent. of it may be removed; if the percentage is 0.09, about 30 per cent. may be removed; if the percentage is only 0.05, there is usually none of it removed. If exceptionally pure lime, containing not more than 0.5 per cent. of silica and only traces of sulphur, is used, the sulphur in the finished steel may be reduced as low as 0.03 per cent.

A small percentage of phosphorus passes back from the slag into the metal when ferro-manganese or spiegeleisen is added, the phosphorus in the slag being reduced by the carbon and the manganese. The agitation caused by the production of CO gas, when ferro or spiegel is added, throws the metal into intimate contact with the slag, and assists the reduction of the phosphorus. This reduction is called the "rephosphorisa-

tion " of the metal, and, in order to lessen the reaction, as much as possible of the slag is poured off before adding ferro or spiegel.

If mild steel is required, ferro-manganese is charged into the converter; for medium or hard steel, molten spiegel-eisen is added in the ladle. At the end of the after-blow the metal is highly oxidised, and before adding the ferro or spiegel it is often partly deoxidised by charging red-hot, grey, hematite pig iron, rich in carbon and silicon, into the converter.

The *chemical reactions* are shown by the following equations:—

As in the acid Bessemer process, the elements which are required to be removed from the pig iron are oxidised by the oxygen contained in the air forced through the molten metal.

$$C + O = CO.$$

Carbon and oxygen yield carbon monoxide.

$$C + O_2 = CO_3$$

Carbon and oxygen yield carbon dioxide.

The gases CO and CO2 escape into the air.

$$Si + O_2 = SiO_2$$

Silicon and oxygen yield silica.

Silica and lime form silicate of lime, which remains in the converter as slag.

$$2\text{Ca}O + \text{Si}O_2 = 2\text{Ca}O, \text{Si}O_2.$$

Lime and silica yield silicate of lime.

$$Mn + O = MnO.$$

Manganese and oxygen yield manganous oxide.

The manganous oxide enters into the slag and helps to keep the slag basic.

 $S + O_{s} = SO_{s}$

Sulphur and oxygen yield sulphur dioxide.

The sulphur dioxide is a gas, and it escapes to the air.

Oxides of iron are formed, and they also enter into the slag.

Fe + O = FeO.

Iron and oxygen yield ferrous oxide. $2\text{Fe} + 3O = \text{Fe}_2O_3$.

Iron and oxygen yield ferric oxide.

/Sulphur trioxide is formed by the action of ferric oxide.

 $9 \operatorname{Fe}_{2} O_{3} + S = 6 \operatorname{Fe}_{3} O_{4} + S O_{3}.$

Ferric oxide and sulphur yield magnetic and sulphur trioxide.

The sulphur trioxide combines with lime in the slag.

 $SO_3 + CaO = CaSO_4.$

Sulphur trioxide and lime yield calcic sulphate.

Nearly all the sulphur eliminated from the pig iron goes into the slag.

 $2P + 50 = P_2O_5.$

Phosphorus and oxygen yield phosphoric acid.

The phosphoric acid combines with the lime and remains in the slag as phosphate of lime.

 $P_2O_5 + 4CaO = 4CaO_1P_2O_5.$

Phosphoric acid and lime yield tetra-calcic-phosphate or phosphate of lime.

BASIC BESSEMER SLAG

The slag resulting from the basic Bessemer process is of much value as a fertiliser, because it contains a high percentage of phosphorus.

The following is an example of the composition of the slag :-

Components.			Percentages.
Phosphoric acid			19
Manganous oxide .			4
Magnesia			6
Lime		. !	49
Oxide of iron			14
Silica, alumina, sulphur,	etc.	.	8
			100

Compare this composition with that of basic openhearth slag given on page 55.

The slag is broken up and ground to a fine powder.

	 _	Acid Siemens and Bessemer.	Basic Siemens.	Basic Bessemer
Silicon .		• 2.0	1.0	1.0
Phosphorus		0.05	1.75	2 6
Sulphur .	. •	0.05	0.06	0.07
Manganese		0.75	1.75	1.2
Carbon .		3.5	3.5	3.6

• Summary.—The compositions of the pig irons used in the different processes which have been described are here placed side by side for comparison.

The best qualities of steel for guns, machinery, etc.,

are made by the acid Siemens process. Good quality steel can also be made by the acid Bessemer'process; but as this process is not so easily controlled, the exact quality of steel required cannot be obtained with certainty.

The Bessemer process is more rapid than the Siemens; thus it is more economical for the manufacture of large quantities of steel.

Mild steel for rails, ship, and bridge material, etc., is, if the composition of the pig iron is suitable, generally manufactured by the Bessemer process, acid or basic, according to the composition of the pig iron obtainable.

The composition of the pig irons for the acid processes and for the basic Siemens must approximate closely to what is given in the tables.

The pig iron for the basic Bessemer may contain more phosphorus and sulphur, but the percentage of sulphur cannot be increased without a more than corresponding increase of phosphorus. For example, if the percentage of sulphur is 0.1, the iron must contain about 3.3 per cent. of phosphorus to provide sufficient heat for its elimination.

Additional heat may be obtained in the Bessemer process by adding the required amount of lime in a highly heated or even molten state, and by passing the air, used for blowing, through a chamber filled with coke, on to which petroleum is allowed to drip. Combustible gases are thus obtained, which, on being mixed with air, burn in the converter and raise the temperature of the metal. This adds to the cost of manufacture of the steel, but the additional heat sometimes makes it possible to make use of pig iron with

•a high• percentage of sulphur, which would otherwise be useless for steel-making.

THE ELECTRIC FURNACE

Melting iron ore and pig iron by means of heat generated by electricity has recently made much progress.

The use of the electric furnace was at first confined to the manufacture of the highest classes of steel, but it is now being developed for refining iron for all qualities of steel, and for smelting iron ore.

Pig iron is melted in an open-hearth furnace, heat being obtained from electrodes let down through the roof of the furnace.

A more intense heat is produced in an electric furnace than by any other means of heating, and thus more of the impurities contained in the iron can be eliminated.

CHAPTER X

TREATMENT OF STEEL INGOTS

If the steel has not been sufficiently deoxidised by the addition of ferro-manganese or spiegeleisen, it will be "wild" or "boiling," and throw off sparks from the ingot mould after it is teemed.

The steel may be quieted by throwing small pieces of aluminium into the moulds. But even when quiet, the fluid steel contains a very large quantity of gases, in volume (at atmospheric pressure) 50 to 75 times that of the metal.

The gases are called occluded gases or gases in occlusion, and they consist chiefly of CO and H. Occluded gases have been mentioned in connection with crucible steel (page 32).

As the ingot cools, it solidifies first on the outside, and also gradually contracts. The fluid centre to some extent settles down to fill up the void caused by contraction and the void caused by the escape of some of the gases. As the fluid centre flows downwards, it forms a hollow at the top of the ingot which is called a "pipe" or "piping"; this is shown in fig. 14.

When the top is solidified, the ascending gases given off from the fluid steel are unable to escape. The gases collect under great pressure and form "blowholes" or "cavities" at the top of the ingot, as shown in fig. 14.

Thus the top of an ingot is unsound, and it is cut off and remelted as scrap.

A method of improving the soundness of an ingot is by "stoppering the ingot." That is, the mould is not

quite filled with steel, and sand is thrown on top of the steel. plate is laid on top of the sand, a bar is passed through the two lugs of the mould, and a wedge is driven in between the plate and the bar. The top of the ingot does not then solidify as quickly as when exposed to the air, and the gases have more time in which to escape. purities in the steel are concentrated in the portion of the ingot which remains the longest in a fluid condition—that is, in the centre. a chemical analysis is made of drillings taken from the centre of an ingot, higher percentages of carbon, phosphorus, and sulphur are found than from drillings near the outside. Consequently, the outside is more malleable than the centre; this is



FIG.14 STEEL INGOT

an advantage when the ingot is being forged or rolled.

When the ingot has solidified sufficiently, so that the outside crust is strong enough to contain the fluid interior, the mould is lifted off; this is called "stripping" the ingot. In this condition the ingot cannot be forged, as the crust would be broken and liquid steel would squirt out.

If the ingot is allowed to stand until it is quite solid, the outside will be too cold for forging, and it will have to be reheated.

Ingots are reheated in *reheating furnaces*, which are either coal fired or heated by the combustion of producer gases.

SOAKING PITS

In order that ingots may be cooled more evenly and be ready for forging without the trouble and the expenditure of fuel necessary to reheat them, they are lowered into holes in the ground called "soaking pits."

The pits are arranged in sets, which are a few inches wider and deeper than the ingot.

Fig. 15 is a sketch showing two soaking pits.

In the beginning the heat from the ingots is absorbed in giving heat to the brickwork lining of the pits, so that when these ingots are taken out, they have to be reheated before they can be forged.

When the pits are well heated, heat is reflected from the brickwork on to the ingot, and during the time of solidification of the interior of the ingot the exterior is maintained at a white heat. Just as the interior becomes solid, the ingot is in the best condition for forging—slightly hotter in the centre than on the outside. Ingots reheated in a reheating furnace are in the reverse condition—hotter on the outside than in the centre. The disadvantages of soaking pits are :-

That it is necessary to take heat from the ingots to first heat the pits, so that the first lot of ingots have to be reheated.

The difficulty of keeping up a regular supply of

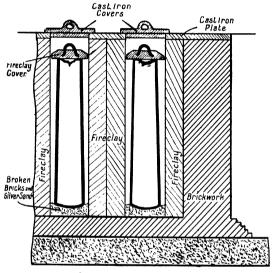


FIG.15. SOAKING PITS.

ingots so that they shall not remain for too long or too short a time in the pits.

For these reasons it is now usual to lower the ingots into furnaces which are called soaking furnaces; these are heated by producer gases and worked on the regenerative system. They are practically reheating furnaces sunk into the ground, and owing to there being little heat lost by radiation, they require only a small quantity of fuel.

FLUID COMPRESSION

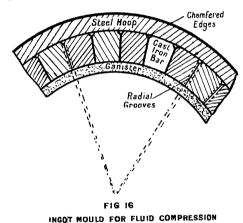
The soundness of an ingot may be improved by subjecting the fluid steel in the mould to a very high pressure. The pressure squeezes some of the occluded gases from the fluid as water is squeezed from a sponge, and the remaining gases being compressed, occupy smaller spaces within the mass of the metal. the particles of steel are forced into more intimate contact with each other, and the grain is made finer and more homogeneous. The numbers of the blowholes may not be much reduced by compression, but it is evident that their sizes must be reduced. For example, a pressure of 5 tons per square inch is equivalent to a pressure of 761 atmospheres; this pressure would compress a bubble of gas into $\frac{1}{\sqrt{6}}$ of its natural volume, or $\frac{1}{6}$ of its diameter. It has been found that pressures up to 2 tons per square inch have no beneficial effect on the steel, so pressures of 5 to 10 tons per square inch are applied. Such high pressures cannot be applied to steel cast in ordinary cast-iron ingot moulds, so special and expensive moulds have to be made.

The moulds are made of forged steel hoops, rough turned and bored, lined all round the inside circumference with cast-iron bars placed vertically and close together. The edges of the bars next to the hoops are chamfered off; the radial grooves, cut in the sides of the bars, connect with the spaces formed by the chamfering so as to permit the escape of gases from top to bottom of the mould. An inner lining of ganister is plastered on to the inner laces of the bars.

Fig. 16 shows a sectional plan of a portion of the

mould. The bottom is closed by a cast-iron plate covered with fireclay, and the top of the mould consists of a cast-iron ring, into which is fitted with a slight clearance a cast-iron plug faced on its lower side with nucleicks.

When hydraulic pressure is applied to the plug, a large quantity of gases escapes from the mould with a roaring sound, and the ingot shortens until its length



is about 10 per cent. less than an ingot cast in the ordinary manner. It is not necessary to cut off the top of a pressed ingot, so there is no waste of metal.

A pressed ingot shows slightly better results in testing for elastic limit, tensile strength, and elongation, and, as the grain of the steel is more homogeneous than that of an unpressed ingot, there is less risk of formation of cracks in cooling and reheating.

The process of staid compression is too slow and too costly to be applied for ordinary commercial rolled

steel, and it is used only in the manufacture of such special steel as is required for guns, crank and propellor shafts, etc.

EFFECTS OF HAMMERING, ROLLING, AND PRESSING STEEL

When steel is poured into a cold mould, the portion next to the mould is immediately solidified and forms a thin outer shell. As heat from the interior escapes through this shell, steel is continually being solidified and, so to speak, "frozen" on to the outer shell.

As the whole mass of metal contracts, approximately in proportion to the decrease of temperature, the fluid steel in the centre performs two functions. It continues to freeze on to the outer shell, and it also endeavours to fill the void in the centre caused by contraction.

The effect is that the steel in the interior of an ingot has a loose texture, and it is defective.

To explain this in another way:—The outer shell of an ingot is immediately formed, and its dimensions are not materially altered when the metal is cold. But as there has been a considerable decrease of volume, the ingot must have either a hollow centre or be of loose texture.

The volume of steel when cold is about 6 per cent. less than when fluid; so the amount of contraction of an ingot of rectangular section, 15 inches \times 14 inches, is equivalent to a cavity of about $3\frac{1}{2}$ inches diameter in its centre.

The greater the size of an ingot the coarser will be the grain in the centre; therefore the centre requires the most forging in order to force the particles of steel into intimate contact with each other.

But, as force has to be applied from the outside, it is difficult to properly forge the interior of an ingot. A pressure is more effective than a blow in transmitting force from the outside to the centre.

If an ingot of mild steel could be removed from a soaking pit or a soaking furnace at the exact time that its centre is at a "welding heat"—that is, a temperature most suitable for welding—the particles of steel in the centre might be welded together by a forging press, and a steel with a fine grain would be produced.

It is, however, always uncertain that the centre is at a welding heat during the process of forging.

Ingots which have to be reheated before forging, cannot be brought to a welding heat in their centres.

An ingot of high carbon steel which does not weld is generally more defective in the centre than an ingot of low carbon steel.

• The blow of a steam hammer is too rapid to permit of the pressure being transmitted from the surface to the centre, where it is the most needed. The difference in the effect of a blow and a squeeze in forging an ingot is easily seen. When an ingot is hammered, the energy is absorbed in spreading the surface, and the interior may remain quite unaffected. The effect of the surface being extended more than the interior is to make the end of a bar or an ingot of the shape as shown by A, and of section shown by B, fig. 17.

When an ingot is squeezed, as by a hydraulic forging press, the outside, on account of long contact with cold masses of metal, loses its heat more rapidly than the

84 THE MANUFACTURE OF IRON AND STEEL

centre, and flows less easily than the hotter centre portion; the centre is thus squeezed out and the end is of the shape shown at C and section D.

When an ingot is rolled in a rolling mill, it is not squeezed out in the same way as by a forging press,

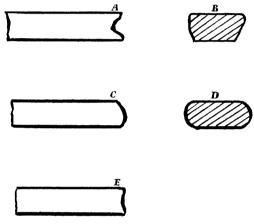


FIG.17.
EFFECTS OF HAMMERING ROLLING AND PRESSING

because the surfaces of the rolls are moving in the same direction in which the bar lengthens, and the rolls drag forward the outer surfaces in confact with them, so the end of a rolled bar will be shaped as E. If the ingot is rolled between plain rolls and not in grooves, which prevent it from spreading laterally, the centre will be squeezed so that the section will be of the same shape as D.

CHAPTER XI

EFFECTS OF ADDING OTHER METALS TO STEEL

Steel readily forms an alloy with most metals, and a small quantity of added metal makes a great difference in its properties.

Manganese.—Some manganese is necessary in steel to counteract a tendency to red shortness. It acts as a deoxidiser. Mild steel ingots containing 0.2 per cent. only of manganese are usually unsound. As the proportion increases, the ingots become sounder; but if the proportion of manganese is over 1 per cent., it becomes detrimental, as the power of elongation of the steel then commences to be reduced. Steel with 2½ per cent. to 7 per cent. of manganese is extremely brittle, but with over 7 per cent. up to 18 per cent., the alloy becomes practically a new metal, which is called "manganese steel"; this possesses great strength and elasticity combined with hardness.

Aluminium is often added to steel, not with the object of forming an alloy, but because of the action which the metal has been found to have on molten steel. Molten steel contains dissolved oxide of iron which diminishes its fluidity and its strength. As the steel cools, the oxide of iron, by the action of carbon, is to some extent reduced, and CO gas is evolved. This

gas causes an ebullition of the molten metal, and it is a cause of blowholes. A small addition of aluminium increases the fluidity of the metal and stops the evolution of gas. The reason for this is, that aluminium has a greater chemical affinity for oxygen than iron has; that is to say, it more readily combines with oxygen than iron does.

The oxide of iron is reduced, and alumina, which separates from the metal as slag, is formed. If too much aluminium is added, it will not be all separated, and there will be weak spots in the steel.

Aluminium has the effect of preventing blowholes; but as it stops the evolution of not only CO gas, but of other occluded gases—that is, hydrogen and nitrogen—it increases the coarseness of the grain of the cast ingot. This coarseness, however, nearly disappears as the ingot is being forged.

Nickel increases the tensile strength and ductility of steel.

An alloy of nickel and steel is now largely used, and it is a splendid material for forgings for the moving parts of machinery.

Nickel steel containing 30 per cent. of nickel can easily be drawn out into wire, and as this large percentage of nickel renders the steel almost non-corrosive, nickel steel is well adapted for ship's hawsers and marine electric cables, which are subject to the corrosive action of salt water.

Chromium.—In small quantities, chromium slightly raises the tensile strength of steel, but it also slightly diminishes its ductility. When added in large quantities, the steel becomes brittle.

Chromium is generally added to steel in conjunction with nickel, for guns, armour plates, and armour-piercing projectiles; the proportions being:—

Carbon, 0.4 per cent.; chromium, 1 per cent.; nickel, 2 per cent.

Chromium makes steel hard, and nickel increases its elasticity.

Vanadium.—As an alloy, vanadium has, for quantity used, the most powerful influence of all alloys on the properties of steel. 0.2 per cent. of vanadium raises the elastic limit and tensile strength of mild steel by about 50 per cent. It is used in the manufacture of the highest classes of tool steel, so called "self-hardening steel."

Steel under continual vibration or under variable strains, such as the piston and connecting rods of an engine, which are alternately under tension and compression, becomes brittle or "fatigued"; the addition of a small percentage of vanadium enables steel to resist this deterioration.

Titanium is a deoxidiser, and it also absorbs nitrogen; so a small quantity added to fluid steel in the ingot mould will assist in the production of a sound casting.

Tungsten or wolfram alloyed with high carbon steel renders it hard, and tools made of this alloy have improved wearing properties.

It also renders steel retentive of magnetism, arg is therefore used in the manufacture of permanar magnets.

g not

Tungsten is used in Germany in the composiof the the "A" tubes—the inner tubes—of guns. Je more

CHAPTER XII

MECHANICAL TESTING OF STEEL

There are two classes of tests to be applied:—

- 1. Hot tests.—The steel is heated to a welding heat to find out if it is free from "red shortness," and if it has good welding qualities.
- 2. Cold tests.—To find out if it is free from "cold shortness," and to ascertain the tensile strength, elasticity, etc.

DEFINITIONS

Tensile strength (or tenacity) is the maximum stress which a bar of a material can sustain, without breaking, when a pulling force is applied gradually in the direction of its length.

It is usually expressed in tons per square inch of cross section.

n Elasticity is the quality which enables a material to mturn to its original form or length on being released actiona force tending to alter its form or length. For

Chile, a metal bar may be stretched up to a certain, raises \ a testing machine, and on being released it will diminish its original length; a steel spring may be the steel force, but its elasticity will cause it to spring

back and straighten itself when the force is released. The act of springing back is called the *resilience* of the spring.

Elastic limit (or limit of elasticity) is the maximum stress which a material can bear without being stretched so much that it cannot return to its original length.

Permanent set.—If a material is stretched beyond its elastic limit, it receives a permanent extension of length which is called "permanent set." A material in this condition is injured and is more liable to "fatigue," which is brittleness caused by vibration or variable stresses, than a material which has not been stretched beyond its elastic limit.

Elongation is the amount of increase in length which a metal can undergo when subjected to a stress sufficient to break it up.

Contraction of area is the amount of reduction of area which takes place at the point of fracture when a metal bar is broken by a tensile stress.

• Yield point is the point at which, when testing a metal bar under a tensile stress just exceeding the elastic limit, the bar suddenly and permanently elongates by a considerable amount without any added increase of stress.

Ductility is the quality which enables a metal to hold together without being injured when subjected to squeezing and stretching, as when rolled in a rolling mill or being drawn out into wire.

• Malleability is the quality which enables a metg not endure hammering when being forged without of the cracked or broken.

be more

STRESS DIAGRAM

An automatic diagram can be taken from a testing machine of the tensile stress and the elongation of a bar, up to the point of fracture.

In fig. 18 the percentage elongations are set out on

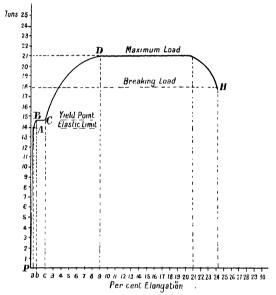


FIG 18. TESTING STEEL STRESS DIAGRAM.

the horizontal line, and the stresses in tons per square 1. inch on the vertical line.

act. As the stress is gradually applied, the bar slightly $C_{i,a}$ ates until, as shown by the diagram, the load is raises i. The point A marks the elastic limit, and the diministrate i it as is the percentage elongated at that point. The steer point there has been little elongation, and

it has been uniform with the increase of load. Beyond the point A the elongation is not uniform. Between 14 and $14\frac{1}{2}$ tons, from A to B, there is a sudden increase in the elongation, and at B the percentage etc. gation is represented by Pb.

Pb is more than twice Pa, so the increase of elongation due to the extra load of $\frac{1}{2}$ -ton, from 14 to $14\frac{1}{2}$ tons, is more than double the total elongation due to the load of 14 tons.

At the point B, suddenly without any addition to the load, there is a great increase in the elongation, from B to C. B marks the "yield point." $Pc = about 5 \times Pa$.

At the point C the elongation ceases, but when a further load, which should be applied gradually, is added, the elongation increases up to the point D, which marks the maximum load (in this case, 21 tons), which the bar will bear. From the point D the bar goes on elongating, the elongation up to the point D baving reduced its sectional area (see fig. 20, page 93), until it finally breaks at H.

The maximum breaking load at II is less than the maximum tensile stress (18 against 21 tons), as, owing to the contraction of area at the point of fracture, a less load is then required to break the bar.

In ordinary commercial testing the yield point is generally taken as the elastic limit, as it is more easily ascertained by the "drop of the beam" of the testitar machine. The yield point is not the true elastic lg not but it is very near it.

To find the elactic limit accurately, the pribe more pair of dividers should be held in the

marks on the bar (elongation marks, see figs. 19 and 20, page 93). When it is seen that a slight elongation takes place, take the load off and see if the marks return to their original distance apart. If they do, slightly increase the load and again release it; and so on, until the load required to cause a very slight permanent set is determined.

Test-pieces

The pieces of steel to be tested are of circular or rectangular section; the circular section is preferable, as the contraction in area after fracture can be more exactly measured. For plates and angle bars, however, it is necessary to cut strips of rectangular section.

Fig. 19 shows sketches of a piece cut from a plate, before and after testing.

If the thickness is $\frac{1}{2}$ -inch, the width of the parallel portion should be 1 inch; this gives a cross sectional area of $\frac{1}{2}$ square inch.

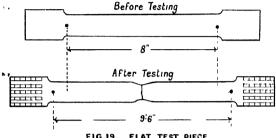
Before the piece is tested, marks are punched on it 8 inches apart; after fracture the pieces are pressed close together and the distance between the marks measured. The distance in excess of 8 inches is the amount of the elongation; the percentage of elongation can then be calculated. The bar has been elongated tu. from 8 inches to 9.6 inches—that is, an elongation of acathaper cent.

ble, e.g. 20 is a sketch of a test-piece of circular section, rais, a te. and after testing.

dimip its antre punch marks are to be made within the the st. force, be h is of the smallest diameter. In this case,

the distance between the marks has been extended from 2 inches to 21 inches—an elongation of 25 per cent.

The length of the parallel portion under test must be



FLAT TEST PIECE

longer with mild steel than with hard steel. If the length is too short, the natural flow of the metal before rupture will be retarded, and the maximum breaking load will be greater than the true breaking load of a longer test-piece. The parallel portion in pieces of

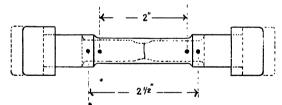


FIG.20. TEST PIECE, CIRCULAR SECTION.

circular section may be shorter than in those of rectangular section, as the contraction is more regular with a circular section. For hard steel containing not less than 0.6 per cent. of carbon, the length of the parallel portion of the test-piece need not be more than 2 inches.

To Calculate the Tensile Strength of a Test-piece

Divide the load at which it breaks by its original sectional area.

Example.—A test-piece, 0.75-in. diameter, is broken under a load of 15.5 tons, what is its tensile strength?

$$.75 \times .75 \times .7854 = .4417$$
:

$$\frac{15.5}{4417} = 35.1 =$$
tensile strength in tons per sq. in.

To simplify the calculations for tensile strength, a testpiece of circular section may be turned of such a diameter that it will be necessary only to multiply the load, which is read off from the beam of the testing machine in lbs., by 2 and divide by 1000 to obtain the result in tons per square inch.

To Find this Diameter

Let x =sectional area in sq. ins. and y =total load in lbs.;

$$\therefore \frac{y}{x}$$
 = tensile strength in lbs. per sq. in.

and $\frac{y}{x \times 2240}$ = tensile strength in tons per sq. in.

It is required that

$$\frac{y}{x \times 2240} = \frac{2y}{1000}.$$

Then

$$x = \frac{1000}{4480} = 2232$$
 sq. in. = sectional area of test-piece.

Let d = required diameter of test-piece, then $d^2 \times .7854 = .2232$;

.:
$$d = .533$$
 in.

Now, with a test-piece of 533-inch diameter, if the breaking load is 17,420 lbs., the tensile strength is 34.04 tons per square inch.

Micrometer.—For accuracy the diameter should be measured with an instrument called a "screw micrometer," by means of which the diameter can be ascertained to within $\frac{1}{1000}$ of an inch.

*• To Find the Percentage Elongation

Example.—Original distance between marks

on test-piece = 8 ins.

Distance between marks after

breaking test-piece = 9.6 ins.

Difference = 1.6 in.

∴ Percentage elongation =
$$\frac{1.6 \times 100}{8} = 20$$
.

To Find the Percentage Contraction of Area of a Test-piece.

Example.—Diameter of piece before testing = '533 in.

Diameter of piece when broken = '34 in.

$$.533 \times .533 \times .7854 = .2232$$
 sq. in.

$$34 \times 34 \times 7854 = 0908 \text{ sq. in.}$$

Difference = 1324 sq. in.

$$\therefore \frac{1324 \times 100}{2232} = 59.3 = \text{percentage contraction of area.}$$

TEST FOR WELDING AND HOT WORKING

Take two pieces of steel about 1 inch square and weld them together as shown at A B in fig. 21. Punch a

 $\frac{5}{8}$ -inch hole at C, and while still red-hot, expand the hole with tapered drifts until it is about $2\frac{1}{2}$ inches diameter.

The steel should show no sign of opening at the weld, and the edges of the expanded portion should be smooth and without cracks.

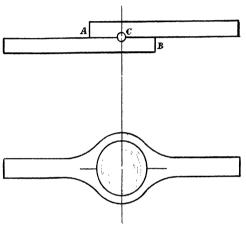


FIG. 21. TEST FOR WELDING

COLD BEND TESTS FOR MILD STEEL PLATES

A strip, $1\frac{1}{2}$ inch wide, is cut lengthways or crosswise from a plate, heated to a cherry-red colour, and cooled in water at 82° F.

When cold, the strip is to be bent over a round bar, the diameter of which is three times the thickness of the strip, without showing any cracks.

CHAPTER XIII

HEAT TREATMENT OF STEEL

When steel containing 0.25 per cent. or more of carbon is heated to redness and suddenly cooled, it becomes hard.

The influence which heating to various temperatures has upon steel may be shown by the following experiment:—

Take a bar of tool steel about 1 foot long and $\frac{3}{4}$ -inch diameter and cut notches with a chisel at intervals of 1 inch throughout its length. Heat one end of the bar in such a manner that it will be at a welding heat at that end, and that there shall be diminishing degrees of redness along the bar, until at the other end there is no appearance of redness.

Now quench the bar in cold water, break off pieces at each notch and compare the fractures. The piece which has been heated to a welding heat will have a coarse grain and will be very brittle. The grain becomes finer with each succeeding piece until the fracture is as that of porcelain; after that the last two or three fractures, which have been heated to lower temperatures, will show a slightly coarser grain.

The part which has the finest grain is the strongest

part of the steel bar, so the object of heat treatment is to obtain the finest possible grain.

If a piece of steel is heated to a welding heat and allowed to cool naturally, it will have a coarse grain and will be brittle; but if the same steel is well hammered or pressed in a forging press when at a welding heat, it will have a fine grain and will be ductile.

HARDENING

There are conditions depending on the temperature of carbon in steel which are called "cement carbon" and "carbon in the hardening state." The carbon passes from the cement to the hardening state by an increase of temperature, and from the hardening state to the cement by a decrease of temperature.

Brinnel, in his experiments with steel containing 0.5 per cent. carbon, found that on heating there was a particular temperature at which there was a retardation in the rate of heating, and at this temperature, which he denoted by the letter W, the carbon changed from the cement to the hardening state.

Also, on cooling steel which had been heated above W, there was a particular temperature at which there was a retardation in the rate of cooling, and at this temperature, which is denoted by the letter V, the carbon changed back from the hardening state to the cement. The temperature V is about 30° C. less than the temperature W.

At the temperature W the steel, in passing from the cement to the hardeing state, becomes of the finest possible grain that can be obtained with that particular

steel. It is then in the best condition for hardening, and is hardened by quenching in cold water. If heated above W the grain again becomes coarse, and if quenched at this higher temperature the steel will be brittle.

When hardened at the temperature W, the steel has its maximum hardness combined with its maximum tensile strength. In hard to medium steels the temperature W is between 650° and 730° C.; in mild steels the temperature W is higher.

ANNEALING

The object of annealing is to remove, as much as possible, internal stresses in the material which have been set up by rolling and forging.

The effect of annealing is to make the steel soft for filing or machining, and to give it its maximum ductility and highest elastic limit. The best temperature for annealing is a temperature above V, but below W; a bar heated to this temperature must be allowed to cool slowly.

Annealed steel has slightly less tensile strength than steel hardened at temperature W, but it has greater ductility and a higher elastic limit.

TEMPERING.

The hardening given to steel by quenching in water, at temperature W, is not suitable for all purposes, the brittleness produced by hardening is redu "tempering"; the 'temper' being made 'particular purpose for which the steel is r

is effected by heating the steel to a temperature very much below that required for hardening; the steel is then either quenched or allowed to cool naturally.

Tempering reduces the brittleness and hardness, and increases the ductility and elastic limit; the texsile strength is not materially altered.

PRACTICAL TEMPERING OF STEEL

When a steel is stated to be of high, low, or medium "temper," it does not mean that it has been tempered to a high, low, or medium degree of hardness; it means that it is a high, low, or medium carbon steel capable of taking a high, low, or medium degree of hardness.

Thus, 1.5 per cent. carbon steel would be called "high temper" steel, and 0.3 per cent. carbon would be called "low temper."

In tempering, the steel should be first hardened by heating to a dull red heat and quenching in water. The surface is then filed bright and gradually heated by laying it on a piece of red-hot iron, or in any other convenient way. The surface then becomes oxidised and changes in colour as the temperature is raised: the colours in succession are:—.

Indicating a temperature

Colour.	suitable for tempering :-		
Dark blue.			
Light blue		Springs, saws.	
the Eurple		Axes, chisels for cut-	
At the		ting iron or steel.	
cement to then to dark brown		Taps, drills.	
possible grain that straw .		Lathe tools, files.	

When the colour indicates that the right temperature has been reached, the steel is either quenched or allowed to cool in the air. If the whole of the metal is required to be of the same degree of hardness, it is air cooled; but in the case of cutting tools, only the cutting edge requires tempering. A tool is heated to a dull red at the cutting end; this extreme end only is quenched and filed bright. The end then becomes reheated by heat conducted from the rest of the tool, and when the cutting edge shows the required colour, the whole tool must be quenched.

The degree of hardness given to the steel will depend not only on the temperature to which it is heated, but on the rapidity with which it is cooled by quenching.

Quenching in mercury, cold brine, or cold water, has a greater hardening effect than quenching in hot water, oil, or molten lead.

Quenching in oil.—The effect of quenching in oil is generally to increase the elasticity of steel. Springs and saws, which should be elastic, but which are not required to be very hard, are quenched in oil.

Quenching in lead.—This has practically no effect on mild steel, but it slightly improves the tensile strength, elastic limit, elongation, and contraction of area of very hard steel.

Pyrometer.—For exact measurements of the temperature of steel when annealing, tempering, and hardening, an instrument called a "pyrometer" is used.

INDEX.

Acid steel, 31, 36. Elastic limit, 89. - Bessemer process, 58. Elasticity, 88. - open-hearth process, 39. Electric furnace, 75. Acids, 36. Elongation, 89, 95. Air blast in blast furnace, 11. Bessemer converter, 59. Fatigue of metals, 57, 87, 89. Alloy, 1. Ferric ore, 6. Alumma, 36, 86. - oxide, 3. Aluminium, 2, 34, 85. Ferro-manganese, 33, 35, 48. Annealing steel, 99. - analysis of, 46. Atomic weights, 2. Ferrous ore, 6. - oxide, 3. Bases, 36. Ferrous-ferric ore, 6. Basic Bessemer ore, 19. Fettling, 23, 24. bricks, 51. materials, 24. lining. 51, 66.materials, 50. Fluid compression, 80. Flux, 15. Furnace, blast, 11. - open-hearth process, 50. - steel, 37. - cementation, 28. Bessemer converter, 58. - electric, 75. - lining, 59, 66. - for crucible steel, 31. - process, 35, 58, 66. - lining, acid open-hearth, 43. Best tap, 24, 53. -- basic open-hearth, 51. Blast furnace, 9. - puddling, 22. — gases, 20. - reheating, 78. Blowing engines, 14. - reverberatory, 24. - Siemens open-hearth, 39. Calcination, advantages of, 7. - soaking, 78. Calcining kiln, 7. - tapping, 9. Carbon, chemical colour test for, 47. - dioxide, 4 Gangue of ore, 6. monoxide, 3. Ganister, 43. - percentages of, in steel, 27. Gas producer, 38. Carbonic acid gas, 4. Gases, blast-furnace, 17. Cementation boxes, 28. - in occlusion, 76. - furnace, 28. - occluded, 32, 76. process of, 28. Grain of metal, 20. Chromium, 86. Cleveland ironstone, 6, 19. Hardening steel, 98. Coke, 15. Heat, Bessemer blow, 64, 70. Told short, 4, 27. Hematite ore, 6, 25, 45.

— pig iron, 19, 46. traction of area, 89, 92. Liggter, Bessemer, 58. Hot-blast stove, 12, or surface-blown, 62. the urple Ingots, fluid compression of, 80. ing process, 57. - gases in, 76. At the - stoppering, 77. cement to the to - treatment of, 76. 102

possible grain that

INDEX

Iron, cast, 17.	Resilience, 89.
orcs, 6. •	Reverberatory furnace, 24.
oxides, 3.	, ,
— pig, 17, 19.	Sand, white or silver, 43.
— — analysis of, 19, 44, 73.	Short, cold, 4, 27.
wrought, 22, 34.	— red, 4, 27.
T 11 1 100	Siemens acid process, 36, 38.
Lead tempering, 101.	- basic process, 50.
Limestone, 15, 69.	Silica, 4.
- analysis of, 51.	Silicon, 4.
Limit of clasticity, 89.	Slag, acid Bessemer, 65.
Lining of Bessemer converter, 59, 66.	- acid Siemens, 49.
- of furnace, acid open-hearth, 43.	— basic Bessemer, 72.
— — basic open-hearth, 50.	- basic Siemens, 55.
Magnesita 51	- blast furnace, 17.
Magnesite, 51.	— wool, 19.
Magnetic oxide, 3.	Smelting, 9.
Magnetite ore, 6.	Soaking furnace, 79.
Malleability, 89. Manganese, 2, 3, 28, 85	— pits, 78.
manganese, 2, 5, 20, 65	Spiegeleisen, 35, 48.
steel, 85. Micrometer, 95	- analysis of, 46.
Micrometer, 95.	Steel, acid. 36.
Mixer, 60.	annealing, 99.
Neutral course, 52.	basic, 37.
Nickel, 2, 86.	- blister, 28. - crucible, 30.
1110111, 2, 00.	
Occluded gases, 32, 76.	— double shear, 30 hardening, 98.
Occlusion, gases in, 76.	- lead tempering, 101.
Oil tempering, 101.	- mild, analysis of, 34.
Open-hearth furnace, 39.	oil tempering, 101.
Ore, calcination of, 7.	- percentage of carbon in, 27.
- Cleveland, 6.	- single shear, 30.
— ferric, 6.	— tempering, 99.
- ferrous, 6.	Stove. hot-blast, 12.
- terrous-ferric, 6.	,
hematite, 6, 45.	Tempering, 99.
- magnetite, 6.	- in lead, 101.
- non-fluxing, 16.	— in oil, 101.
- reduction of, 16.	Tenacity, 88.
- self-fluxing, 16.	Tensile strength, 88, 91.
Oxide, ferric, 3.	Test-pieces, 92.
— ferrous, 3.	Testing of steel, 88.
— magnetic, 3.	Tests, cold, 39, 88, 96.
	— hot, 88, 95.
Permanent set, 89.	- welding, 95.
Phosphorus, 4.	Titanium, 2, 87.
Pig iron, 17, 19.	Tungsten, 2, 87.
— — analysis of, 19, 44, 73.	Tuyeres, 11, 59, 67.
Pottery mine, 25, 53.	
Producer gas, 38.	Vanadium, 2, 87.
Puddling furnace, 22.	
Purple ore, 25.	Wheelswarf, 28.
Pyrometer, 101.	Wolfram, 2, 87.
	Wrought iron, analy
Red short, 4, 27.	\
Regenerator, 12, 39.	Yield point. ^



PRINTED BY
NEILL AND COMPANY, LIMITED,
EDINBURGH.

A SHORT LIST OF

SCIENTIFIC BOOKS

UBLISHED BY

E. & F. N. SPON, Limited,

57, Haymarket, London, S.W.

SOLE ENGLISH AGENTS for the Books of --

MYRON C. CLARK, NEW YORK SPON & CHAMBERLAIN, NEW YORK

$\mathbf{P}I$	XGE.		Р	AGE
	2	LOGARITHM TABLES		
	2	Manufactures		2.2
	4	MARINE ENGINEERING		20
	4 :	MAIERIALS		28
	5 1	MATHEMATICS		28
	2	MECHANICAL ENGINEERING		20
	7	METMIURGY		2.
	9	METRIC TABLES		3 3
	11	MINERALOGY AND MINING		2.4
	1.2	MISCELLANEOUS		4.5
	1.2	Model Making		2:
	13	MUNICIPAL ENGINEERING		30
	Lą .	NAVAL ARCHITECTURE		26
	14	ORGANIZATION	•	30
	19	Physics	•	36
	19	Price Books	•	37
	20	RAH WAY ENGINEERING	• •	38
ī.	20	SANITATION		39
	21	STRUCTURAL DESIGN		J-5
	21	TELEGRAPH CODES		45
	22	USEFUL TABLES		46
	48	WARMING: VENTILATION		4.5
	25	WATER SUPPLY		42
		2 4 4 5 2 7 9 11 12 13 14 19 19 10 20 21 21 21 22 48	LOGARITHM TABLES MANUFACIURES MARINE ENGINEERING MATERIALS MECHANICAL ENGINEERING MECHANICAL ENGINEERING METHIURGY METHIURGY MINERALOGY AND MINING MISCELLANEOUS MODEL MAKING MUNICIPAL ENGINEERING MAVAI ARCHITECTURE MORGANIZATION PHYSICS PHYSICS ANI WAY ENGINEERING SANIATION 20 RAH WAY ENGINEERING LOGANIZATION TELEGRAPH CODES LUSEPUL TABLES WARMING: VENTILATION 25 WATER SUPPLY	LOGARITHM TABLES MANUFACIURES MARINE ENGINEERING MATHEMATICS MECHANICAL ENGINEERING METHIURGY METHIURGY MOBEL HARING MOBEL HARING MUNICIPAL ENGINEERING MUNICIPAL ENGINEERING MUNICIPAL ENGINEERING MANAI ARCHITECTURE ORGANIZATION PHYSICS PRICE BOOKS RAILWAY ENGINEERING AND PRICE BOOKS SAMIATION TIEGRAPH CODES USEPUL TABLES WARMING: VENTILATION 48 WARMING: VENTILATION LOGANIZATION LOGANIZATION LOGANIZATION LOGANIZATION MUNICIPAL ENGINEERING LOGANIZATION LOGANIZA

All books are bound in cloth unless otherwise stated.

NOTE: The Prices in this Catalogue apply to books sold in the United Kingdom only.

P.R. 937]

AGRICULTURE

- Hemp. A Practical Treatise on the Culture for Seed and Fibre. By S. S. Boyce. 13 illus., 112 pp., crown 8vo. (New York, 1900.) 2s. 6d. net.
- Farm Drainage. By H. F. French. 100 illus., 284 pp., crown 8vo. (New York, 1904.) 4s. 6d. net.
- Spices and How to Know Them. By W. M. Gibbs. With 47 plates, including 14 in colours, 179 pp., 8vo. (New York, 1909.) 15s. net.
- Talks on Manures. By J. Harris. New edition, 366 pp., crown 8vo. (New York, 1893.) 6s. 6d. net.
- Coffee, its Culture and Commerce in all Countries. By C. G. W. Lock. 11 plates, 274 pp., crown 8vo. (1888.) 12s. 6d.
- Sugar, a Handbook for Planters and Refiners. By the late J. A. R. Newlands and B. E. R. Newlands. 236 illus., 876 pp., demy 8vo. (1909.) £1 5s. net.
- Hops, their Cultivation, Commerce and Uses. By P. L. Simmonds. 1.43 pp., crown 8vo. (1877.) 4s. 6d.
- Estate Fences, their Choice, Construction and Cost. By A. **Vernon.** Re-issue, 150 illus., 420 pp., 8vo. (1909.) 8s. 6d. net.

ARCHITECTURE AND BUILDING

- Engineering Work in Public Buildings. By R. O. Allsop. 77 illus., 168 pp., demy 4to. (1912.) 12s. 6d. net.
- The Hydropathic Establishment and its Baths. By R. O. Allsop. 8 plates, 107 pp., demy 8vo. (1891.) 5s.
- The Turkish Bath, its Design and Construction. By R. O. Allsop. 27 illus., 152 pp., demy 8vo. (1890.) 6s.
- Public Abattoirs, their Planning, Design and Equipment. By R. S. Ayling. 33 plates, 100 pp., demy 4to. (1908.) 8s. 6d. net.
- The Builder's Clerk. By T. Bales. Second edition, 92 pp., fcap. 8vo. (1904.) is. 6d.
- Glossary of Technical Terms used in Architecture and the Building Trades. By G. J. Burns. 136 pp., crown 8vo. (1895.) 3s. 6d.
- Chimney Design and Theory. By W. W. Christie. Second edition, 54 illus., 200 pp., crown 8vo. (New York, 1902.) 12s. 6d. net.

- Approximate Estimates. By T. E. Coleman. Third edition \$1 pp., oblong 32mo, leather. (1907.) 5s. net.
- Stable Sanitation and Construction. By T. E. Coleman. 183 illus., 226 pp., crown 8vo. (1897.) 6s.
- House Plans and Building Construction for General Contractors and House Builders. By M. M. Dustman. 511 illus., 239 pp., oblong folio. (New York, 1912.) 8s. 6d. net.
- Architectural Examples in Brick, Stone, Wood and Iron. By W. Fullerton. Third edition, 245 plates, 254 pp., demy 4to. (1908.) 15s. net.
- Bricklaying System. By F. B. Gilbreth. 240 illus., 321 pp., 8vo. (New York, 1909.) 12s. 6d. net.
- **Field System.** By **F. B. Gilbreth.** 194 pp., 12mo, leather. (*New York*, 1908.) 12s. 6d. net.
- The Building Trades Pocket Book. Compiled by R. Hall. 12mo, with diary. 1s. net.
- The Economics of Contracting. By D. J. Hauer. 10 illus., viii + 269 pp., crown 8vo. (New York, 1911.) 12s. net.
- The Clerk of Works' Vade Mecum. By G. G. Hoskins. Seventh edition, 52 pp., Icap. 8vo. (1901.) 1s. 6d.
- Paint and Colour Mixing. By A. S. Jennings. Fourth edition, 14 col. plates, 190 pp., 8vo. (1910.) 5s. net.
- A Handbook of Formulæ, Tables, and Memoranda for Architectural Surveyors. By J. T. Hurst. Fifteenth
- edition, new impression, 112 illus., viii + 512 pp., royal 32mo, roan. (1912.) 5s. net.
- Quantity Surveying. By J. Leaning. Fifth edition, new impression, 936 pp., 8vo. (1912.) £1 5s. net.
- Builders' Quantities. By H. M. Lewis. 6 illus., 44 pp., crown 8vo. (S. & C. Series, No. 40.) (1911.) 1s. 6d. net.
- Obstruction to Light. A Graphic Method of determining Problems of Arcient Lights. By H. B. Molesworth. 9 folding plates, 4to. (1902.) 6s. net.
- Suburban Houses. A series of practical plans. By J. H. Pearson. 46 plates and 12 pp. text, crown 4to. (1905.) 7s. 6d. net.
- Solid Bitumens, their Physical and Chemical Properties. By S. F. Peckham. 23 illus., 324 pp., 8vo. (New York, 1909.) £1 1s.

- Roman Architecture, Sculpture and Ornament. By G. B. Piranesi. 200 plates, reproduced in facsimile from the original. 2 vols., imperial folio, in wrappers. (1900.) £2 2s. net.
- The Seven Periods of English Architecture, defined and illustrated. By E. Sharpe. Third edition, 20 steel plates, royal 8vo. (1888.) 12s. 6d.
- Our Factories, Workshops and Warehouses, their Sanitary and Fire-Resisting Arrangements. By B. H. Thwaite. 183 illus., 282 pp., crown 8vo. (1882.) 9s.
- Elementary Principles of Carpentry. By T. Tredgold and J. T. Hurst. Eleventh edition, 48 plates, 517 pp., crown 8vo. (1904.) 12s. 6d.
- Treatise on the Design and Construction of Mill Buildings. By W. G. Tyrrell. 652 illus., 490 pp., demy 8vo. (New York, 1911.) 178. net.
- Practical Stair Building and Handrailing. By W. H. Wood. 32 plates, 91 pp., crown 4to. (1894.) 10s. 6d.
- Spons' Architects' and Builders' Pocket Price-Book and Diary, 1913. Edited by Clyde Young. Revised by Stanford M. Brooks. 10mo, green leather cloth (size $6\frac{1}{2}$ in. by $3\frac{\pi}{4}$ in. by $\frac{1}{2}$ in. thick). 230 pp., with Diary showing a week at an opening. 28. 6d. net.
- Spons' Practical Builders' Pocket Book. Edited by Clyde Young and Stanford M. Brooks. 72 illus., 400 pp, 16mo, leather cloth (1913). 5s. net.

ARTILLERY

- Guns and Gun Making Material. By G. Ede. Crown 8vo. (1889.) 6s.
- Treatise on Application of Wire to Construction of Ordnance. By J. A. Longridge. 180 pp., 8vo. (1884.) £15s.
- The Progress of Artillery: Naval Guns. By J. A. Long-ridge. 8vo, sewed. (1896.) 2s.
- The Field Gun of the Future. By J. A. Longridge. 8vo, sewed. (1892.) 2s. 6d.

AVIATION

The Atmosphere, its Characteristics and Dynamics. By F. J. B. Cordeiro. 35 illus., 129 pp., small 4to. (New York, 1910.) 10s. 6d. net.

- Theory and Practice of Model Aeroplaning. By V. E. Johnson. 61 illus., 150 pp., crown 8vo. (1910.) 38. 6d. net.
 - The Gyroscope, An Experimental Study. By V. E. Johnson. 34 illus., 40 pp., crown 8vo. (S. & C. Series, No. 22.) (1911.) 18. 6d. net.
- Natural Stability and the Parachute Principle in Aeroplanes. By W. Le Maitre. 34 illus., 48 pp., crown 8vo. (S. & C. Series, No. 39.) (1911.) 1s. 6d. net.
- How to Build a 20-ft. Bi-plane Glider. By A. P. Morgan. 31 illus., 60 pp., crown 8vo. (S. & C. Series, No. 14.) (New York, 1909.) 18. 6d. net.
- Flight-Velocity. By A. Samuelson. 4 plates, 42 pp., 8vo, sewed. (1906.) 2s. net.
- Resistance of Air and the Question of Flying. By A. Samuelson. 23 illus., 36 pp., 8vo, sewed. (1905.) 2s. net.
- **The Laws of Avanzini.** Laws of Planes moving at an angle in air and water. By Lieut.-Col. **R. de Villamil.** 2 folding plates, 3 illus., 23 pp., super royal 8vo, sewed. (1912.) 2s. net.
- Aeroplanes in Gusts, Soaring Flight and Aeroplane Sfability. By S. L. Walkden. 4 plates, 47 illus., xvi + 188 pp., 8vo. (1912.) 7s. 6d. net.

BRIDGES, ARCHES, ROOFS, AND STRUCTURAL DESIGN

- Strains in Ironwork. By Henry Adams. Fourth edition, 8 plates, 65 pp., crown 8vo. (1904.) 5s.
- Designing Ironwork. By Henry Adams. Second series, 8vo, sewed.
 - Part I. A Steel Box Girder. (1891.) od. net.
 - " II Built-up Steel Stanchions. (1901.) 1s. 3d. net.
 - " III. Cisterns and Tanks. (1902.) is, net. " IV. A Fireproof Floor. (1903.) is, net.
- Columns and Struts. Theory and Design. By Wm. Alexander. 101 illus., xii + 265 pp., demy 8vo. (1912.) 10s. 6d. net.
- A Practical Treatise on Segmental and Elliptical Oblique or Skew Arches. By G. J. Bell. Second edition, 17 plates, 125 pp., royal &vo. (1906.) £1 is. net.

Economics of Construction in relation to Framed Structures. By R. H. Bow. Third thousand, 16 plates, 88 pp., 8vo.

(1873.) 5s.

Theory of Voussoir Arches. By Prof. W. Cain. Third edition, 201 pp., 18mo, boards. (New York, 1905.) 2s. net.

New Formulæ for the Loads and Deflections of Solid Beams

and Girders. By **W. Donaldson.** Second edition, 8vo. (1872.) 4s. 6d.

- Plate Girder Railway Bridges. By M. Fitzmaurice. 4 plates, 104 pp., 8vo. (1895.) 6s.
- Pocket Book of Calculations in Stresses. By E. M. George. 66 illus., 140 pp., royal 32mo, half roan. (1895.) 3s. 6d. Strains on Braced Iron Arches and Arched Iron Bridges.
- By A. S. Heaford. 39 pp., 8vo. (1883.) 6s. **Tables for Roof Framing.** By G. D. Inskip. Second edition, 451 pp., 8vo, leather. (New York, 1905.) 12s. 6d.

net.

Stresses in Girder and Roof Frames, for both dead and

- hve loads, by simple Multiplication, etc. By F. R. Johnson. 28 plates, 215 pp., crown 8vo. (1894.) 6s.
- A Graphical Method for Swing Bridges. By B. F. La Rue. 4 plates, 104 pp., 18mo, boards. (New York, 1904.) 2s. net.
- Bridge and Tunnel Centres. By J. B. McMasters. Illustrated, 106 pp., 18mo, boards. (New York, 1893.) 2s. net.
- Notes on Cylinder Bridge Piers and the Well System of Foundations. By J. Newman. 144 pp., 8vo. (1893.) 6s.
- Calculation of Columns. By T. Nielsen. 4 plates, 36 pp., 8vo. (1911.) 4s. 6d. net.
- A New Method of Graphic Statics applied in the Construction of Wrought Iron Girders. By E. Olander. 16 plates, small folio. (1887.) 10s. 6d.
- Steel Bar and Plate Tables. Giving Weight of a Lineal Foot of all sizes of L and T Bars, Flat Bars, Plates, Square and Round Bars. By E. Read. On large folding card. (1911.) 1s. net.
- Reference Book for Statical Calculations. By F. Ruff. With diagrams, 140 pp., crown 8vo. (1906.) 5s. net.
- Suspension Bridges and Cantilevers. By D. B. Steinmann. vii + 185 pp., 18mo, boards. (Van Nostrand Series, No. 127.) (New York, 1911.) 2s. net.

- The Strength and Proportion of Riveted Joints. By B. B. Stoney. 87 pp., 8vo. (1885.) 5s.
- The Anatomy of Bridgework. By W. H. Thorpe. 103 illus., 190 pp., crown 8vo. (1906.) 6s. net.

CEMENT AND CONCRETE

- **Portland Cement,** its Manufacture, Testing and Use. By **D. B. Butler.** Second edition, 97 illus., 396 pp., demy 8vo. (1905.) 16s. net.
- Theory of Steel-Concrete Arches and of Vaulted Structures. By W. Cain. Fourth edition, 27 illus., 212 pp., 18mo, boards. (New York, 1906.) 28. net.
- Reinforced Concrete Construction. Elementary Course. By M. T. Cantell. 65 illus., 135 pp., crown 8vo. (1911.) 4s. 6d. net.
- Reinforced Concrete Construction. Advanced Course. By M. T. Cantell. 242 illus., xv1 + 240 pp., super royal 8vo. (1912.) 12s. 6d. net.
- Graphical Reinforced Concrete Design. A series of Diagrams on sheets (measuring 17½ in. by 22½ in.) for Designing and Checking. With 48-page pamphlet. By J. A. Davenport. Complete in roll. (1911.) 58. net.
- Cement Users' and Buyers' Guide. By Calcare. 115 pp., 32mo, cloth. (1901.) 1s. 6d. net.
- Diagrams for Designing Reinforced Concrete Structures. By G. F. Dodge. 31 illus., 104 pp., oblong folio. (New York, 1910.) 178. net.
- Cements, Mortars, and Concretes; their Physical properties. By M. S. Fałk. 78 illus., 176 pp., 8vo. (New York, 1904.) 10s. 6d. net.
- Concrete Construction, Methods and Cost. By H. P. Gillette and C. S. Hill. 310 illus., 690 pp., 8vo. (New York, 1908.) £1 is. net.
- Engineers' Pocket Book of Reinforced Concrete. By E. L. Heidenreich. 164 illus., 364 pp., crown 8vo, leather, gilt edges. (New York, 1909.) 12s. 6d. net.
- Concrete Inspection. By C. S. Hill. 15 illus., 179 pp., 12mo. (New 7 k, 1909.) 4s. 6d. net.

- 8 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- Practical Silo Construction. By A. A. Houghton. 18 illus., 69 pp., crown 8vo. (S. & C. Series, No. 27e) '(New York, 1911.) 1s. 6d. net.
- Moulding Concrete Chimneys, Slate and Roof Tiles. By A. A. Houghton. 15 illus., 61 pp., crown 8vo. (S. & C. Series, No. 28.) (New York, 1911.) 18. 6d. net.
- Moulding and Curing Ornamental Concrete. By A. A. Houghton. 5 illus., 58 pp., crown 8vo. (S. & C. Series, No. 29.) (New York, 1911.) 1s. 6d. net.
 - Concrete Monuments, Mausoleums and Burial Vaults. By A. A. Houghton. 18 illus., 65 pp., crown 8vo. (S. &
- C. Series, No. 31.) (*New York*, 1911.) 1s. 6d. net.

 Concrete Floors and Sidewalks. By A. A. Houghton.

 8 illus., 63 pp., crown 8vo. (S. & C. Series, No. 32.) (*New York*, 1911.) 1s. 6d. net.
- Moulding Concrete Baths, Tubs, Aquariums and Natatoriums. By A. A. Houghton. 16 illus., 64 pp., crown 8vo. (S. & C. Sfries, No. 33.) (New York, 1911.) 1s. 6d. net.
- Concrete Bridges, Culverts, and Sewers. By A. A. Houghton. 14 illus., 58 pp., crown 8vo. (S. & C. Series, No. 34.) (New York, 1912.) 1s. 6d. net.
- Constructing Concrete Porches. By A. A. Houghton. 18 illus., 62 pp., crown 8vo. (S. & C. Series, No. 35.) 1s. 6d. net.
- Moulding Concrete Flower-Pots, Boxes, Jardinières, etc. By A. A. Houghton. 8 illus., 52 pp., crown 8vo. (S. & C. Series, No. 36.) (New York, 1912.) 1s. 6d. net.
- Moulding Concrete Fountains and Lawn Ornaments. By A. A. Houghton. 14 illus., 56 pp., crown 8vo. (S. & C. Series, No. 37.) (New York, 1912.) 1s. 6d. net.
- Pp., crown 8vo. (New York, 1908.), 6s. 6d. net.
- Concrete and Reinforced Concrete. By H. A. Reid. 715 illus., 884 pp., royal 8vo. (New York, 1907.) £1 is. net.
- Theory and Design of Reinforced Concrete Arches. By A. Reuterdahl. 41 illus., 126 pp., 8vo. (New York, 1908.) 8s. 6d. net.
- Specification for Concrete Flags. Issued by the Institution of Municipal and County Engineers. Folio, sewed. (1911.) 2s. 6d. net.

Practical Cement Testing. By W. P. Taylor. With 142 illus., 329 pp., demy 8vo. (New York, 1906.) 12s. 6d. net.

Concrete Bridges and Culverts. By H. G. Tyrrell. 66 illus., 251 pp., crown 8vo, leather. 12s. 6d. net.

CIVIL ENGINEERING

Canals, Surveying.

(See also Irrigation and Water Supply.)

- Practical Hints to Young Engineers Employed on Indian Railways. By A. W. C. Addis. With 14 illus., 154 pp., 12mo. (1910.) 38 6d. net.
- Levelling, Barometrie, Trigonometrie and Spirit. By I. O. Baker. Second edition, 15 illus., 145 pp., 18mo, boards. (New York, 1903.) 2s. net.
- Punjab Rivers and Works. By E. S. Bellasis. 47 illus., viii + 64 pp., folio, cloth. (1912.) 8s. net.
- Notes on Instruments best suited for Engineering Field Work in India and the Colonies. By W. G. Bligh. 65 illus., 218 pp., 8vo. (1899.) 7s. 6d.
- Practical Designing of Retaining Walls. By Prof. W. Cain. Fifth edition, 14 illus., 172 pp., 18mo, boards. (New York, 1908.) 2s. net.
- **Land Area Tables.** By **W. Codd.** Sheet mounted on linen, in cloth case, with explanatory booklet. 3s. 6d.
- The Maintenance of Macadamised Roads. By T. Cod-• rington. Second edition, 186 pp., 8vo. (1892.) 7s. 6d.
- The Civil Engineers' Cost Book. By Major T. E. Coleman, R.E. xii + 289 pp., Pocket size (6½ × 3½ in.), leather cloth. (1912.) 5s. net.
- Retaining Walls in Theory and Practice. By T. E. Coleman. 104 illus., 160 pp., crown 8vo. (1909.) 5s. net.
- On Curved Masonry Dams. By W. B. Coventry. 8vo, sewed. (1894.) •2s.
- A Practical Method of Determining the Profile of a Masonry Dam. By W. B. Coventry. 8vo, sewed. (1894.) 2s. 6d.
- The Stresses on Masonry Dams (oblique sections). By W. B. Coventry. 8vo, sewed. (1894.) 2s.
- Handbook of Cost Data for Contractors and Engineers. By H. P. Gillette. 1,854 pp., crown 8vo, leather, gilt edges. (New 'r.k,*1911.) £1 1s. net.

- Rock Excavation, Methods and Cost. By H. P. Gillette. Second edition in preparation.
- High Masonry Dams. By E. S. Gould. With illus., 88 pp., 18mo, boards. (New York, 2nd. edit., 1905.) 2s. net.
- Railway Tunnelling in Heavy Ground. By C. Gripper. 3 plates, 66 pp., royal 8vo. (1879.) 7s. 6d.
- Levelling and its General Application. By T. Hollóway. Third edition in preparation.
- Waterways and Water Transport. By J. S. Jeans. 55 illus., 520 pp., 8vo. (1890.) 98. net.
- Table of Barometrical Heights to 20,000 Feet. By Licut.-Col. W. H. Mackesy. 1 plate, 24 pp., royal 32mo. (1882.) 3s.
- Aid Book to Engineering Enterprise. By E. Matheson. Third edition, illustrated, 916 pp., medium 8vo, buckram. (1898.) (148.
- A Treatise on Surveying. By R. E. Middleton and O. Chadwick. Third edition, royal 8vo. (1911.)
 Part 1. 11 plates, 162 illus., 285 pp. 10s. 6d.
- II. 152 illus, and 2 plates, 340 pp. 10s. 6d.
 A Pocket Book of Useful Formulæ and Memoranda, for Civil and Mechanical Engineers. By Sir G. L. Molesworth and H. B. Molesworth. With an Electrical Supplement
- and H. B. Molesworth. With an Electrical Supplement by W. H. Molesworth. Twenty-sixth edition, 760 illus, 901 pp. royal 32mo, French morocco, gilt edges. (1908.) 5s. net. The Pocket Books of Sir G. L. Molesworth and J. T. Hurst,
- printed on India paper and bound in one vol. Royal 32m6, russia, gilt edges. 10s. 6d. net.
- Metallic Structures: Corrosion and Fouling and their Prevention. By J. Newman. Illustrated, 385 pp., crown 8vo. (1896.) qs.
- Scamping Tricks and Odd Knowledge occasionally practised upon Public Works. By J. Newman. New imp., 129 pp., crown 8vo. (1908.) 2s. net.
- Co-ordinate Geometry applied to Land Surveying. By W. Pilkington. 5 illus., 44 pp., 12mo. (1909.) 1s. 6d. net.
- **Pioneering.** By **F. Shelford.** Illustrated, 88 pp., crown Svo. (1909.) 35, net.
- Topographical Surveying. By G. J. Specht. Second edition, 2 plates and 28 illus., 210 pp., 18mo, boards. (New York 1898.) 2s. net.

- Spons' Dictionary of Engineering, Civil, Mechanical, Military, and Naval. 10,000 illus., 4,300 pp., super royal 8vo. (1874, Supplement issued in 1881.) Complete, in 4 vols. £3 3s. net.
- Surveying and Levelling Instruments. By W. F. Stanley. Fourth edition in preparation.
- Surveyor's Handbook. By T. U. Taylor. 116 illus., 310 pp., crown 8vo, leather, gilt edges. (New York, 1908.) 8s. 6d. net.
- Logarithmic Land Measurement. By J. Wallace. 32 pp. royal 8vo. (1910.) 5s. net.
- The Drainage of Fens and Low Lands by Gravitation and Steam Power. By W. H. Wheeler. 8 plates, 175 pp., 8vo. (1888.) 128. 6d.
- Stadia Surveying, the theory of Stadia Measurements. By A. Winslow. Fifth edition, 148 pp., 18mo, boards. (New York, 1902.) 2s. net.
- Handbook on Tacheometrical Surveying. By C. Xydis. 55 illus., 3 plates, 63 pp., 8vo. (1909.) 6s. net.

CURVE TABLES

- **Grace's Tables for Curves,** with hints to young engineers. 8 figures, 43 pp., oblong 8vo. (1908.) 5s. net.
- Railroad Curves and Earthwork. By C. F. Allen. Third edition, 4 plates, 198 pp., 12mo, leather, gilt edges. (*Vece York, 1903.*) 8s. 6d. net.
- Data relating to Railway Curves and Super-elevations, shown graphically. By J. H. Haiste. On folding card for pocket use. 6d. net.
- Tables for setting-out Railway Curves. By C. P. Hogg. A series of cards in neat cloth case. 48, 6d.
- Tables for setting out Curves for Railways, Roads, Canals, etc. By A. Kennedy and R. W. Hackwood. 32mo. 2s. net.
- **Spiral Tables.** By **J. G. Sullivan**. 47 pp., 12mo, leather. (*New York, 1908.*) 6s. 6d. net.
- Tables for Setting out Curves from 101 to 5 000 feet radius.

 By H. A. Cutler and F. J. Edge. Royal 32mo 2s. net.
- Tables of Parabolic Curves for the use of Railway Engineers, and others. 7. G. T. Allen. Fcap 16mo. 4s.

Transition Curves. By W. G. Fox. 18mo, boards. (New York.) 2s. net.

DICTIONARIES

- Technological Dictionary in the English, Spanish, German and French Languages. By D. Carlos Huelin Y Arssu.
 - Vol. I. English-Spanish-German-French. 600 pp. (1906.) 10s. 6d. net.
 - Vol. II. German-English-French-Spanish. 720 pp. (1908.) 10s. 6d. net.
 - Vol. III. FRENCH-GERMAN-SPANISH-ENGLISH. In preparation.
 - Vol. IV. Spanish-French-English-German. 750 pp. (1910.) 10s. 6d. net.
- Dictionary of English and Spanish Technical and Commercial Terms. By W. Jackson. 164 pp., fcap 8vo. (1911.) 28. 6d. net.
- English-French and French-English Dictionary of the Motor-Car, Cycle and Boat. By F. Lucas. 171 pp., crown 8vo. (1905.) 2s. net.
- Spanish-English Dictionary of Mining Terms. By F. Lucas. 78 pp., 8vo. (1905.) 5s. net.
 - English-Russian and Russian-English Engineering Dictionary. By L. Meycliar. 100 pp., 16mo. (1909.) 2s. 6d. net.

DOMESTIC ECONOMY

- Food Adulteration and its Detection. By J. P. Battershall. 12 plates, 328 pp., demy 8vo. (New York, 1887.) 15s.
- Practical Hints on Taking a House. By H. P. Boulnois. 71 pp., 18mo. (1885.) 1s. 6d.
- The Cooking Range, its Failings and Remedies, By F. Dye. 52 pp., fcap. 8vo, sewed. (1888.) 6d.
- Spices and How to Know Them. By W. M. Gibbs. With 47 plates, including 14 in colours, 179 pp., 8vo. (New York, 1909.) 15s. net.
- The Kitchen Boiler and Water Pipes. By H. Grimshaw, 8vo, sewed. (1887.) 1s. net.

- Cookery and Domestic Management, including economic and middle class Practical Cookery. By K. Mellish. 56 coloured plates and 441 illus., 987 pp., super royal 8vo. (1901.) 16s. net.
- **Spons' Household Manual.** 250 illus., 1,043 pp., demy 8vo. (1902.) 7s. 6d.

Ditto ditto half-bound French morocco, 9s.

DRAWING

- The Ornamental Penman's, Engraver's and Sign Writer's Pocket Book of Alphabets. By B. Alexander. New Impression. Oblong 12mo, sewed. (1912.) 6d. net.
- Slide Valve Diagrams: a French Method for their Construction. By L. Bankson. 18mo, boards. (New York, 1892.) 2s. net.
- A System of Easy Lettering. By J. H. Cromwell. With Supplement by G. Martin. Eleventh edition, 36 pp., oblong 8vo. (New York, 1911.) 2s. net.
- Key to the Theory and Methods of Linear Perspective. By C. W. Dymond, F.S.A. 6 plates, 32 pp., crown 8vo. (S. & C. Series, No. 20.) (1910.) 1s. 6d. net.
- Plane Geometrical Drawing. By R. C. Fawdry. Illustrated, 185 pp., crown 8vo. (1901.) 3s. net.
- Twelve Plates on Projection Drawing. By O. Gueth.
 Oblong 4to. (New York, 1903.) 3s. net.
- Hints on Architectural Draughtsmanship. By G. W. T. Hallatt. Fourth edition, 80 pp., 18mo. (1996.) 1s. 6d. net.
- A First Course of Mechanical Drawing (Tracing). By G. Halliday. Oblong 4to, sewed. 2s.
- A Text-Book of Graphic Statics. By C. W. Malcolm. 155 illus., 310 pp., 8vo. (New York, 1909.) 12s. 6d. net.
- Drawings for Medium-sized Repetition Work. By R. D. Spinney. With 47 illus., 130 pp., 8vo. (1909.) 3s. 6d. net.
- Mathematical Drawing Instruments. By W. F. Stanley.
 Seventh edition, 265 illus., 370 pp., crown 8vo. (1900.)

 5s.
- The Backbone of Perspective. By T. U. Taylor. 40 illus., 56 pp., 18mo coth. (New York, 1911.) 4s. 6d. net.

EARTHWORK

- Tables for Computing the Contents of Earthwork in the Cuttings and Embankments of Railways. By W. Macgregor. Royal Svo. 6s.
- Tables for facilitating the Calculation of Earthworks. By D. Cunningham. 120 pp., royal 8vo. 10s. 6a...
- Grace's Earthwork Tables. 36 double-page tables, 4to. (1907.) 128. 6d. net.
- Earthwork Slips and Subsidences on Public Works. By J. Newman. 240 pp., crown 8vo. (1890.) 7s. 6d.
- Diagrams for the Graphic Calculation of Earthwork Quantities. By A. H. Roberts. Ten cards, fcap., in cloth case. 108 6d net.

ELECTRICAL ENGINEERING

- Practical Electric Bell Fitting. By F. C. Allsop. Tenth edition, 186 illus., including 8 folding plates, 185 pp., crown 8vo. (1903) 38. 6d
- Telephones: their Construction and Fitting. By F. C. Allsop. Eighth edition, new impression, 184 illus., 222 pp., crown 8vo. (1912.) 38, 6d, net.
- Auto-Transformer Design. By A. H. Avery. 25 illus., 60 pp., 8vo. (1909.) 3s 6d. net.
- Principles of Electric Power (Continuous Current) for Mechanical Engineers. By A. H. Bate. 63 illus., 204 pp., crown 8vo. (1905.) (FINSBURY TECHNICAL MANUAL.) 4s. 6d. net.
- Practical Construction of Electric Tramways. By W. R. Bowker. 93 illus., 119 pp., 8vo. (1903.) 6s. net.
- The Electric Motor and its Practical Operation. By E. E. Burns. 78 illus., vi + 91 pp., crown 8vo. (New York, 1912.) 78, net.
- Electrical Ignition for Internal Combustion Engines. By M. A. Codd. 109 illus., 163 pp., crown 8vo. (1911.) 3s. net.
- Design and Construction of Induction Coils. By A. F. Collins. 155 illus., 272 pp., demy 8vo. (New York, 1909.) 128, 6d. net.
- Plans and Specification for Wireless Telegraph Sets. By A. F. Collins. Crown 8vo. (S. & C. Series, Nos. 41 and 42). (New York, 1912.) 1s. 6d. each net.

- PART I. An Experimental Set and a One to Five
 Miles Set. 37 illus., viii + 45 pp.
- PART II. A Five to Ten Mile Set and a Ten to Twenty Mile Set. 63 illus., viii + 72 pp.
- Switchboard Measuring Instruments for Continuous and Polyphase Currents. By J. C. Connan. 117 illus, 150 pp., 8vo. (1908.) 5s. net.
- Electric Cables, their Construction and Cost. By D. Coyle and F. J. O. Howe. With many diagrams and 216 tables, 466 pp., crown 8vo, leather. (1909.) 15s. net.
- Management of Electrical Machinery. By F. B. Crocker and S. S. Wheeler. Eighth edition, 131 illus., 223 pp., crown 8vo. (New York, 1909.) 48, 6d, net.
- Electric Lighting: A Practical Exposition of the Art. By F. B. Crocker. Royal 8vo. (New York.)
 - Vol. I. The Generating Plant. Sixth edition, 213 illus., 470 pp. (1901.) 128. (11. net.
 - Vol. II. Distributing Systems and Lamps. Second edition, 301 illus., 505 pp. (1905.) 128. 6d. net.
- The Care and Management of Ignition Accumulators. By H. H. U. Cross. 12 illus., 74 pp., crown 8vo. (S. & C. Series, No. 19.) (1910.) 1s. 6d. net.
- Elements of Telephony. By A. Grotch. 51 illus, 90 pp., crown 8vo. (S. & C. Serries, No. 21.) (1911.) 18, 6d, net.
- Elementary Telegraphy and Telephony. By Arthur Crotch. New impression, 238 illus, viii + 223 pp., 8vo. (FINSBURY TECHNICAL MANUAL.) (1912.) 4s. 6d. net.
- Electricity and Magnetism in Telephone Maintenance. By G. W. Cummings. 15 illus, 137 pp., 8vo. New York, 1908.) 6s 6d. net.
- Grouping of Electric Cells. By W., F. Dunton. 4 illus. 50 pp., fcap. 8vo. (1906) 1s. 6d. net.
- Wireless Telegraphy for Intending Operators. By C. K. P. Eden. 20 illus, 80 pp., crown 8vo (S. & C. Series, No. 24.) In preparation.
- Magnets and Electric Currents. By Prot. J. A. Fleming. Second edition, 136 illus., 417 pp., crown 8vo. (1902.) 5s. net.
- Notes on Design of Small Dynamo. By George Halliday.

 Second edition, 8 plates, 8vo. (1895.) 28, 6d.
- Practical Alternating Currents and Power Transmission. By N. Harn Jan. 172 illus., 375 pp., crown 8vo. (New York, 1906.) 108. (d. net.

- 16 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- Making Wireless Outfits. By N. Harrison. 27 illus., 61 pp., crown 8vo. (S. & C. SERIES, No 11.) (New York, 1909.) 1s. 6d. net.
- Wireless Telephone Construction. By N. Harrison. 43 illus., 73 pp., crown 8vo. (S. & C. Series, No. 12.) (New York, 1909.) 18, 6d. net.
- **Testing Telegraph Cables.** By Colonel **V. Hoskiær.** Ihrd edition, 11 illus., viii + 75 pp., crown 8vo. (1889.) 4s. 6d.
- Long Distance Electric Power Transmission. By R. W. Hutchinson. 136 illus., 345 pp., crown 8vo. (New York, 1907.) 12s. 6d. net.
- Theory and Practice of Electric Wiring. By W. S. Ibbetson. 119 illus., 366 pp., crown 8vo. (1909.) 5s. net.
- Practical Electrical Engineering for Elementary Students. By W. S. Ibbetson. 61 illus., 155 pp., crown 8vo. (1910.) 38. 6d. net.
- Form of Model General Conditions recommended by The Institution of Electrical Engineers for use in connection with Electrical Contracts. New edition in preparation.
- Telegraphy for Beginners. By W. H. Jones. 19 illus., 58 pp., crown 8vo. (New York, 1910) 2s. net.
- A Handbook of Electrical Testing. By H. R. Kempe. Seventh edition, 285 illus, 706 pp. demy 8vo. (1908.) 18s, net.
- Electromagnets, their Design and Construction. By A. N. Mansfield. 36 illus., 155 pp., 18mo, boards. (New York, 1901.) 2s. net.
- Telephone Construction, Methods and Cost. By C. Mayer. With Appendices on the cost of materials and labour by J. C. Slippy. 103 illus., 284 pp., crown 8vo. (New York, 1908.) 128. 6d. net.
- Storage Batteries, Stationary and Portable. By J. P. Niblett. 22 illus., 80 pp., crown 8vo. (New York, 1911.) 2s. 6d. net.
- House Wiring. By T. W. Poppe. 73 illus., 103 pp., 12mo, limp. (New York, 1912.) 2s. 6d. net.
- Practical Electrics: a Universal Handybook on Every Day Electrical Matters. Seventh edition, 126 illus., 135 pp., 8vo. (S. & C. Series, No. 13.) (New York, 1902.) 1s. 6d. net.
- Electroplating. By H. C. Reetz. 62 illus., 99 pp., crown 8vo. (New York, 1911.) 2s. net.

- Wiring Houses for the Electric Light. By N. H. Schneider. 40 illus., 85 pp., crown 8vo. (S. & C. Serries, No. 25.) (New York, 1911.) 18. 6d. net.
- Induction Coils. By N. H. Schneider. Second edition, 79 illus., 285 pp., crown 8vo. (New York, 1901.) 48 6d. net.
- Electric Gas Lighting. By N. H. Schneider. 57 illus., 101 pp., crown 8vo. (S. & C. Series, No. 8.) (New York, 1901.) 1s. 6d. net.
- How to Install Electric Bells, Annunciators and Alarms. By N. H. Schneider. 50 illus., 63 pp., crown 8vo, limp. (S. & C. Series, No. 2.) (New York, 1905.) 1s. 6d. net.
- Modern Primary Batteries, their construction, use and maintenance. By N. H. Schneider. 54 illus., 94 pp., crown 8vo. (S. & C. Serres, No. 1.) (New York, 1905.) 1s. 6d net.
- Practical Engineers' Handbook on the Care and Management of Electric Power Plants. By N. II. Schneider. 203 illus, 274 pp., crown 8vo (Vew York, 1906.) 58, net.
- Electrical Circuits and Diagrams, illustrated and explained. By N. H. Schneider. 8vo. (S. & C. SERIES, Nos. 3 and 4.) (New York.)
 - No. 3, Part 1. New edition in preparation. No. 4, Part 2. 73 pp. (1909.) 18. 6d. net.
- Electrical Instruments and Testing. By N. H. Schneider. Third edition, 133 illus, 239 pp., crown 8vo. (New York, 1907.) 4s. 6d. net.
- Experimenting with Induction Coils. By N. H. Schneider. 26 illus., 73 pp., crown 8vo (S. & C. SERIFS, No. 5.) (New York, 1906.) 1s. 6d. net.
- Study of Electricity for Beginners. By N. H. Schneider. 54 illus., 88 pp., crown 8vo. (S. & C. Series, No. 6.) (New York, 1905.) 18. 6d. net.
- Wiring Houses for the Electric Light: Low Voltage Battery Systems. 44 illus., 86 pp., crown 8vo. (S. & C. SERIES, No. 25.) (New York, 1911.) 1s. 6d. net.
- By N. H. Schneider. 23 illus., 85 pp., crown 8vo. (S. & C. Series, No. 26) (New York, 1911.) 18. 6d. net.
- Dry Batteries: how to Make and Use them. By a Dry Battery Expert. With additional notes by N. H. Schneider. 30 illus., 59 pp., crown 8vo. (S. & C. Series, No. 7.) (New York, 1905.) 6d. net.

- 18 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- The Diseases of Electrical Machinery. By E. Schulz. Edited, with a Preface, by Prof. S. P. Thompson. 42 illus., 84 pp., crown 8vo. 2s. net.
- Electricity Simplified. By T. O. Sloane. Tenth edition, 29 illus., 158 pp., crown 8vo. (New York, 1901.) 4s. 6d.
- How to become a Successful Electrician. By T. O. Sloane.
 Third edition, 4 illus., 202 pp., crown 8vo. (New York, 1899.) 4s. 6d. net.
- Electricity: its Theory, Sources and Applications. By J. T. Sprague. Third edition, 100 illus., 658 pp., crown 8vo. (1892.) 7s. 6d. net.
- Telegraphic Connections. By C. Thom and W. H. Jones. 20 plates, 59 pp., oblong 8vo. (New York, 1892.) 3s. 6d. net.
- Dynamo Electric Machinery. By Prof. S. P. Thompson.
 Seventh edition, demy 8vo. (Finsbury Technical Manual.)
 Vol. I. Continuous-Current Machinery. With 4
 - coloured and 30 folding plates, 573 illus., 984 pp. (1904.) £1 10s. net.

 Vol. H. Alternating Current Machinery. 15
 - coloured and 24 folding plates, 546 illus., 900 pp. (1905.) £1 108. net.
- Design of Dynamos (Continuous Currents). By Prof. S. P. Thompson. 4 coloured and 8 folding plates, 243 pp., demy 8vo. (1903.) 12s. net.
- Schedule for Dynamo Design, issued with the above 6d. each, 4s. per doz., or 18s. per 100, net.
- Curves of Magnetic Data for Various Materials. A reprint on transparent paper for office use of Plate I from Dynamo Electric Machinery, and measuring 25 in. by 16 in. 7d. net.
- The Electromagnet. By C. R. Underhill. 67 illus., 159 pp., crown 8vo. (New York, 1903.) 68, 6d, net.
- Practical Guide to the Testing of Insulated Wires and Cables. By H. L. Webb. Fifth edition, 38 illus., 118 pp., crown 8vo. (New York, 1902.) 4s. 6d. net.
- Wiring Rules. With Extracts from the Board of Trade Regulations and the Home Office Regulations for Factories and Workshops. Issued by The Institution of Electrical Engineers. Sixth edition, 42 pp., 8vo, sewed. (1911.) 6d. net.

FOREIGN EXCHANGE

- English Prices with Russian Equivalents (at Fourteen Rates of Exchange). English prices per lb., with equivalents in roubles and kopecks per pood. By A. Adiassewich. 182 pp., fcap. 32mo, roan. (1908.) 1s. net.
- English Prices with German Equivalents (at Seven Rates of Exchange). English Prices per lb., with equivalents in marks per kilogramme. By St. Koczorowski. 95 pp., fcap. 32mo, roan. (1909.) 1s. 4net.
- English Prices with Spanish Equivalents. At Seven Rates of Exchange. English prices per lb., with equivalents in pesetas per kilogramme. By S. Lambert. 95 pp., 32mo, roan. (1910.) 1s. net.
- English Prices with French Equivalents (at Seven Rates of Exchange). English prices per lb. to francs per kilogramme. By H. P. McCartney. 97 pp., 32mo, roan. (1907.) 18. net.
- **Principles of Foreign Exchange.** By E. Matheson. Fourth edition, 54 pp., 8vo, sewed. (1905) 3d. net.

GAS AND OIL ENGINES

- The Theory of the Gas Engine. By D. Clerk. Edited by F. E. Idell. Third edition, 19 illus., 180 pp., 18mo, boards. (New York, 1903.) 2s. net.
- Electrical Ignition for Internal Combustion Engines. By M. A. Codd. 109 illus., 163 pp., crown 8vo. (1911.) 38. net.
- The Design and Construction of Oil Engines. By A. II. Goldingham. Third edition, 112 illus., 260 pp., crown 8vo. (New York, 1910.) 10s. 6d. net.
- Gas Engine in Principle and Practice. By A. H. Goldingham. New impression, 107 illus., 195 pp., 8vo. (vew York, 1912.) 6s. 6d. net.
- Practical Handbook on the Care and Management of Gas Engines. By G. Lieckfeld. Third edition, square 16mo. (New York, 1896.) 3s. 6d.
- Elements of Gas Engine Design. By S. A. Moss. 197 pp., 18mo, boards. (New York, 1907.) 2s. net.
- Gas and Petroleum Engines. A Manual for Sciden's and Engineers. By Pr. f. W. Robinson. (FINSBURY FECHNICAL MANUAL.) Third edition in preparation.

Gasolene Engines, their Operation, Use, and Care. By A. Hyatt Verrill. 152 illus., 275 pp., crown 8vo. $\epsilon(New York, 1912.)$ 6s. 6d. net.

GAS LIGHTING

- Gas Analyst's Manual (incorporating Hartley's "Gas Analyst's Manual" and "Gas Measurement"). By J. Abady. 102 illus., 576 pp., demy 8vo. (1992.) 18s. net.
- Gas Works: their Arrangement, Construction, Plant and Machinery. By F. Colyer. 31 folding plates, 134 pp., 8vo. (1881.) 8s. 6d. net.
- Transactions of the Institution of Gas Engineers. Edited by Walter T. Dunn, Secretary. Published annually. 8vo. 10s. 6d. net.
- **Lighting by Acetylene.** By **F. Dye.** 75 illus., 200 pp., crewn 8vo. (1902.) 6s. net.
- A Comparison of the English and French Methods of Ascertaining the Illuminating Power of Coal Gas. By A. J. Van Eijndhoven. Illustrated, crown 8vo. (1897.) 48.
- Gas Lighting and Gas Fitting. By W. P. Gerhard. Third edition, 190 pp., 18mo, boards. (New York, 1904.) 2s. net.
- A Treatise on the Comparative Commercial Values of Gas Coals and Cannels. By D. A. Graham. 3 plates, 100 pp., 8vo. (1882.) 4s. 6d.
 - The Gas Engineer's Laboratory Handbook. By J. Hornby. Third edition, revised, 70 illus., 330 pp., crown 8vo. (1911.) 6s. net.

HISTORICAL AND BIOGRAPHICAL

- Extracts from the Private Letters of the late Sir William Fothergill Cooke, 1836-9, relating to the Invention and Devel panent of the Electric Telegrah; also a Memoir by Latimer Clark. Edited by F. H. Webb, Sec. Inst. E. E. 8v.o. (1895.) 3s.
- A Chronology of Inland Navigation in Great Butain. By H. R. De Salis. Crown 8v. (1897.) 48. 6d.
- A History of Electric Telegraphy to the year 1837. By J. J. Fahie. 35 illus., 542 pp., crown 8vo. (1889.) 2s. net.
- History and Development of Steam Locomotion on Common Roads. By W. Fletcher. '109 iffus., 288 pp., 8vo. 5s.

- Life as an Engineer: its Lights, Shades, and Prospects. By J. W. C. Haldane. New edition, 23 plates, 390 pp., crown 8vo. (1910.) 5s. net.
- Philipp Reis, Inventor of the Telephone: a Biographical Sketch. By Prof. S. P. Thompson. 8vo, cloth. (1883.) 7s. 6d.
- The Development of the Mercurial Air Pump. By Prof. S. P. Thompson. Illustrated, royal 8vo, sewed. (1888.) 1s. 6d.

HOROLOGY

- Witch and Clock Maker's Handbook, Dictionary and Guide. By F. J. Britten. Tenth edition, 450 il us, 492 pp., crown 8vo. (1992.) 5s. net.
- The Springing and Adjusting of Watches. By F. J. Britten. 75 illus., 152 pp., crown 8vo. (1898.) 38, net.
- Prize Essay on the Balance Spring and its Isochronal Adjustments. By M. Immisch. 7 illus., 50 pp., crown 8vo. (1872.) 2s. 6d.

HYDRAULICS AND HYDRAULIC MACHINERY

(See also Irrigation and Water Supply.)

- The Suction Caused by Ships explained in popular language. By E. S. Bellasis. 2 plates, 26 pp., 8vo, sewed. (1912.) 18. net.
- Hydraulics with Working Tables. By E. S. Bellasis. Second edition, 160 illus., xii+311 pp., 8vo. (1911.) 12s. net.
- Pumps: Historically, Theoretically and Practically Considered By P. R. Björling. Second edition, 156 illus., 234 pp., crown 8vo. (1895.) 7s. 6d.
- Pump Details. By P. R. Björling. 278 illus., 211 pp., crown 8vo. (1892.) 7s. 6d.
- Pumps and Pump Motors: A Manual for the use of Hydraulic Engineers. By P. R. Björling. Two vols., 261 plates, 369 pp., royal 4to. (1895.) £1 10s. net.
- Practical Handbook on Pump Construction. By P. R.
 Björling. Second edition, new impression, 9 plates, viii +
 86 pp., crown 8vo. (1912.) 3s. 6d. net.
- Water or Hydraulic Motors. By P. R. Björling. 206 illus., 287 pp., crown evo. 1903.) 98.

- Hydraulic Machinery, with an Introduction to Hydraulics. By R. G. Blaine. Second edition, with 307 illus, 468 pp., 8vo. (FINSBURY TECHNICAL MANUAL.) (1905.) 14s. net.
- Practical Hydraulics. By T. Box. Fifteenth edition, 8 plates, 88 pp., crown 8vo. (1909.) 5s. net.
- Pumping and Water Power. By F. A. Bradley. 51 illus., vn + 118 pp., demy 8vo. (1912.) 4s. 6d. net.
- Hydraulic, Steam, and Hand Power Lifting and Pressing Machinery. By F. Colyer. Second edition, 88 plates, 211 pp., imperial 8vo. (1892.) 10s. 6d. net.
- Pumps and Pumping Machinery. By F. Colyer.
 V l. 1. Second edition, 53 plates, 212 pp., 8vo. (1392.)
 - 10s. 6d. net. V l. II. Second edition, 48 plates, 169 pp., 8vo.
- (1900.) 10s. 6d. net.

 Construction of Horizontal and Vertical Water-wheels.
- By W. Cullen. Second edition, small 4to. (1871.) 5s.
- Donaldson's Poncelet Turbine and Water Pressure Engine and Pump. By W. Donaldson. 2 plates, viii + 32 pp., demy 4to. (1883.) 5s.
- Principles of Construction and Efficiency of Water-wheels. By W. Donaldson. 13 illus., 94 pp., 8vo. (1876) 5s.
- Practical Hydrostatics and Hydrostatic Formulæ. By E. S. Gould. 27 illus., 114 pp., 18mo, boards. (New York, 1903.) 2s. net.
- Hydraulic and Other Tables for purposes of Sewerage and Water Supply. By T. Hennell. Third edition, 70 pp., crown 8vo. (1998.) 4s. 6d. net.
- Tables for Calculating the Discharge of Water in Pipes for Water and Power Supplies. Indexed at side for ready reference. By A. E. Silk. 63 pp., crown 8vo. (1899.) 5s.
- Simple Hydraulic Formulæ. By T. W. Stone. 9 plates, 98 pp., crown 8vo. (1881.) 4s.
- A B C of Hydrodynamics. By Lieut.-Col. R. de Villamil, R.E. (retd.). 48 illus., xi + 135 pp., demy 8vo. (1912.) 6s. net.

INDUSTRIAL CHEMISTRY AND MANUFACTURES

Transaction of the American Institute of Chemical Engineers. Issued annually. 30s. het.

- Perfumes and their Preparation. By G. W. Askinson. Translated from the Third German Edition by I. Fuest. Third edition, 32 illus., 312 pp., 8vo. (New York, 1907.) 12s. 6d. net.
- Brewing Calculations, Gauging and Tabulation. By C. H. Bater. 340 pp., 64mo, roan, gilt edges. (1897.) is. 6d. i.et.
- A Pocket Book for Chemists, Chemical Manufacturers, Metallurgists, Dyers, Distillers, etc. By T. Bayley. Seventh edition, new impression, 550 pp., royal 32mo, roan, gilt edges. (1912.) 5s. net.
- Practical Receipts for the Manufacturer, the Mechanic, and for Home use. By Dr. H. R. Berkeley and W. M. Walker. New impression, 250 pp., demy 8vo. (1912.) 5s. net.
- A Treatise on the Manufacture of Soap and Candles, Lubricants and Glycerine. By W. L. Carpenter and H. Leask. Second edition, 104 illus., 456 pp, crown 8vo. (1895.) 128, 6d.
- A Text Book of Paper Making. By C. F. Cross and E. J. Bevan. Third edition, 97 illus., 411 pp., crown 8vo. (1907.) 12s. 6d. net.
- C.B.S. Standard Units and Standard Paper Tests. By C.
 F. Cross, E. J. Bevan, C. Beadle and R. W. Sindall.
 25 pp., crown 4to. (1903.) 2s. 6d. net.
- **Pyrometry.** By **C. R. Darling.** 60 illus., 200 pp., crown 8vo. (1911.) 5s. net.
- Soda Fountain Requisites. A Practical Receipt Book for Druggists, Chemists, etc. By G. H. Dubelle. Third edition, 157 pp., crown 8vo. (New York, 1905.) 4s. 6d. net.
- Spices and How to Know Them. By W. M. Gibbs. 47 plates, including 14 in colours, 176 pp., 8vo. (New York, 1909.) 15s. net.
- The Chemistry of Fire and Fire Prevention. By H. and H. Ingle. 45 illus, 290 pp., crown 8vo. (1900.) 9s.
- Ice-making Machines. By M. Ledoux and others. Sixth edition, 190 pp., 18mo, boards. (New York, 1906.) 2s. net.
- Brewing with Raw Grain. By T. W. Lovibond. 75 pp., crown 8vo. (1883.) 5s.
- The Chemistry, Properties, and Tests of Precious Stones.

 By J. Mastin. 114 pp., fcap. 16mo, limp leather, gilt top.

 (1911.) 2s. 62: 14.

- Sugar, a Handbook for Planters and Refiners. By the late J. A. R. Newlands and B. E. R. Newlands. 236, illus., 876 pp., 8vo. (1909.) £1 5s. net.
- Principles of Leather Manufacture. By Prof. H. R. Procter. 101 illus., 520 pp., medium 8vo. (1908.) 18s. net.
- Leather Industries Laboratory Handbook of Analytica Vand Experimental Methods. By H. R. Procter. Second edition, 4 plates, 46 illus., 450 pp., demy 8vo. (1908.) 18s. net.
- **Leather Chemists' Pocket Book.** A short compendium of Analytical Methods. By Prof. H. R. Procter. Assisted by Dr. E. Stiasny and H. Brumwell. 4 illus., xiv + 223 pp., 16mo, leather. (1912.) 5s net.
- Theoretical and Practical Ammonia Refrigeration. By I. I. Redwood. Sixth thousand, 15 illus., 146 pp., square 16mo. (New York, 1909.) 4s. 6d. net.
- Breweries and Maltings. By G. Scammell and F. Colyer. Second edition, 20 plates, 178 pp., 8vo. (1880.) 6s. net.
- Factory Glazes for Ceramic Engineers. By H. Rum-Bellow. Folio. Series A. Leadless Sanitary Glazes. (1908.) £2 28. net.
- Spons' Encyclopædia of the Industrial Arts, Manufactures and Commercial Products. 1,500 illus., 2,100 pp., super royal 8vo. (1882.) In 2 vols., cloth. 1,2 2s. net.
- The Absorption Refrigerating Machine. By G. T. Voorhees. 42 illus., 144 pp., narrow crown 8vo. (New York, 1911.) 8s. 6d. net.
- **Tables for the Quantitative Estimation of the Sugars.** By **E. Wein** and **W. Frew.** Crown 8vo. (1896.) 6s.
- The Puering, Bating and Drenching of Skins. By J. T. Wood. 33 illus., xy + 300 pp, demy 8vo. (1912.) 12s. 6d. net.
- Workshop Receipts. For the use of Manufacturers, Mechanics and Scientific Amateurs. New and thoroughly Revised Edition, crown 8vo. (1909.) 38, each net.
 - Vol. I. Acetylene Lighting to Drying. 223 illus., 532 pp.
 - Vol. II DYEING to JAPANNING. 259 illus., 540 pp.
 - Vol. III. Jointing Pipes to Pumps. 256 illus., 528 pp., Vol. IV. Rainwaifr Separators to Wire Rope
 - Splicing. 321 illus., 540 pp.

- Practical Handbook on the Distillation of Alcohol from Farm Products. By F. B. Wright. Second edition, 60 iffus, 271 pp., crown 8vo. (New York, 1907.) 4s. 6d. net.
- The Manufacture of Chocolate and other Cacao Preparations. By P. Zipperer. Second edition, 87 illus., 280 pp., royal 8vo. (1902.) 16s. net.

INTEREST TABLES

- The Wide Range Dividend and Interest Calculator, showing at a glance the Percentage on any sum from One Pound to Ten Thousand Pounds, at any Interest, from 1 per cent. to 12½ per cent., proceeding by ¼ per cent. By A. Stevens. 100 pp., super royal 8vo, cloth. 6s. net. Quarter morocco, cloth sides, 7s. 6d. net.
- The Wide Range Income Tax Calculator, showing at a glance the Tax on any sum from One Shilling to Thousand Pounds, at the Rate of 9d., 1s., and 1s. 2d. in the Pound. By A. Stevens. On folding card, imperial 8vo. 1s. net.

IRRIGATION

- Punjab Rivers and Works. By E. S. Bellasis. Second edition, 47 illus., 65 pp., folio, cloth. (1912.) 8s. net.
- Irrigation Pocket Book. By R. B. Buckley. 419 pp., crown 8vo, leather cloth with rounded corners. (1911.) 12s. 6d. net.
- The Design of Channels for Irrigation and Drainage. By R. B. Buckley. 22 diagrams, 56 pp., crown 8vo. (1911.) 2s. net.
- The Irrigation Works of India. By R. B. Buckley. Second edition, with coloured maps and plans. 336 pp., 4to, cloth. (1905.) £2 25. net.
- Irrigated India. By Hon. Alfred Deakin. With Map, 322 pp., 8vo. (1893.) 8s. 6d.
- Indian Storage Reservoirs, with Earthen Dams. By W. L. Strange. Second edition in preparation.
- The Irrigation of Mesopotamia. By Sir W. Willcocks. 2 vols., 46 plates, 136 pp. (Text super royal 8vo, plates folio.) (1911.) & net.
- Egyptian Irrigation. By Sir W. Willcocks.
- Third edition in preparation.
 - A few copies of the First Edition (1889) are still to be had. Price 15s. no.

- The Nile Reservoir Dam at Assuân, and After. By Sir W. Willcocks. Second edition, 13 plates, super royal 8vo. (1903.) 6s. net.
- The Assuan Reservoir and Lake Moeris. By Sir W. Will-cocks. With text in English, French and Arabic. 5 plates, 116 pp., super royal 8vo. (1904.) 5s. net.
- The Nile in 1904. By Sir W. Willcocks. 30 plates, 200 pp., super royal 8vo. (1904.) 9s. net.

LOGARITHM TABLES

- Aldum's Pocket Folding Mathematical Tables. Four-figure Logarithms, and Anti-logarithms, Natural Sines, Tangents, Cotangents, Cosines, Chords and Radians for all angles from I to 90 degrees. And Decimalizer Table for Weights and Money. On folding card. 4d. net. 20 copies, 6s. net.
- Tables of Seven-figure Logarithms of the Natural Numbers from 1 to 108,000. By C. Babbage. Stereotype edition, 224 pp., medium 8vo. 5s. net.
- Four-Place Tables of Logarithms and Trigonometric Functions. By E. V. Huntington. Ninth thousand, 34 pp., square 8vo, limp buckram, with cut lateral index. (New York, 1911.) 3s. net.
- Short Logarithmic and other Tables. By W. C. Unwin. Fourth edition, small 4to. 3s.
- Logarithmic Land Measurement. By J. Wallace. 32 pp., royal 8vo. (1910.) 5s. net.
- A B C Five-figure Logarithms with Tables, for Chemists. By C. J. Woodward. Crown 8vo. 2s. 6d. net.
- A B C Five-figure Logarithms for general use, with lateral index for ready reference. By C. J. Woodward. Second edition, with cut lateral Index, 116 pp., 12mo, limp leather. 3s. net.

MARINE ENGINEERING AND NAVAL ARCHITECTURE

- Marine Propellers. By S. W. Barnaby. Fifth edition, 5 plates, 56 illus., 185 pp., demy 8vo. (1908.) 10s. 6d. net.
- Marine Engineer's Record Book: Engines. By B. C. Bartley. 8vo, roan. 5s. net.

- The Suction Caused by Ships and the Olympic-Hawke Gollision. By E. S. Bellasis. 1 chart and 5 illus. in text, 26 pp., 8vo, sewed. (1912.) 1s. net.
- Yachting Hints, Tables and Memoranda. By A. C. Franklin. Waistcoat pocket size, 103 pp., 64mo, roan, gilt edges. 1s. net.
- Steamship Coefficients, Speeds and Powers. By C. F. A. Fyfe. 31 plates, 280 pp., fcap. 8vo, leather. (1907.) 10s. 6d. net.
- Steamships and Their Machinery, from first to last. By J. W. C. Haldane. 120 illus., 5,32 pp., 8vo. (1893.) 15s.
- Tables for Constructing Ships' Lines. By A. Hogg. Third edition, 3 plates, 20 pp., 8vo, sewed. (1911.) 3s. net.
- Submarine Boats. By G. W. Hovgaard. 2 plates, 98 pp., crown 8vo. (1887.) 5s.
- Tabulated Weights of Angle, Tee, Bulb, Round, Square, and Flat Iron and Steel for the use of Naval Architects, Shipbuilders, etc. By C. H. Jordan. Sixth edition, 640 pp., royal 32mo, French morocco, gilt edges. (1909.) 7s. 6d. net.
- Particulars of Dry Docks, Wet Docks, Wharves, etc., on the River Thames. Compiled by C. H. Jordan. Second edition, 7 coloured charts, 103 pp., oblong 8vo. (1904.)' 2s. 6d. net.
- Marine Transport of Petroleum. By H. Little. 66 illus. 263 pp., crown 8vo. (1890.) 10s. 6d.
- Questions and Answers for Marine Engineers, with a Practical Treatise on Breakdowns at Sea. By T. Lucas. 12 folding plates, 515 pp., gilt edges, crown 8vo. (New York, 1902.) 8s. net.
- Reed's Engineers' Handbook to the Board of Trade Examinations for certificates of Competency as First and Second Class Engineers. Nineteenth edition, 37 plates, 358 illus., 696 pp., 8vo. 14s. net.
- Key to Reed's Handbook. 7s. 6d. net.
- Reed's Marine Boilers. Third edition, 79 illus., 258 pp., crown 8vo. (1905.) 4s. 6d. net.
- Reed's Useful Hints to Sea-going Engineers. Fourth edition, 8 plates, 50 illus., 312 pp., crown 8vo. (1903.) 3s. 6d. net. **

MATERIALS

- Practical Treatise on the Strength of Materials. By T. Box. Fourth edition, 27 plates, 536 pp., 8vo. (1902.) 12s. 6d. net.
- Treatise on the Origin, Progress, Prevention and Cyre of Dry Rot in Timber. By T. A. Britton. 10 plates, 519 pp., crown 8vo. (1875.) 7s. 6d.
- Solid Bitumens. By S. F. Peckham. 23 illus., 324 pp., 8vo. (New York, 1909.) £1 1s. net.
- Lubricants, Oils and Greases. By I. I. Redwood. 3 plates, ix + 54 pp., 8vo. (1898.) 6s. 6d. net.
- Practical Treatise on Mineral Oils and their By-Products. By I. I. Redwood. 76 illus., 336 pp., demy 8vo. (1897.) 15s.
- Silico-Calcareous Sandstones, or Building Stones from Quartz, Sand and Lime. By E. Stoffler. 5 plates, 8vo, sewed. (1901.) 4s. net.
- Proceedings of the Fifth Congress, International Association for Testing Materials. English edition. 189 illus., 549 pp., demy 8vo. (1910.) Paper, 15s. net.; cloth, 18s. net.

MATHEMATICS

- Imaginary Quantities. By M. Argand. Translated by Prof. Hardy. 18mo, boards. (New York.) 2s. net.
- Text-book of Practical Solid Geometry. By E. H. de V. Atkinson. Revised by Major B. R. Ward, R.E. Second edition, 17 plates, 8vo. (1901.) 7s. 6d.
- Quick and Easy Methods of Calculating, and the Theory and Use of the Slide Rule. By R. G. Blaine. Fourth edition, 6 illus., xii + 152 pp., 16mo, leather cloth. (1912.) 2s. 6d. net.
- Symbolic Algebra, or the Algebra of Algebraic Numbers. By W. Cain. 18mo, boards. (New York.) 2s. net.
- Nautical Astronomy. By J. H. Colvin. 127 pp., crown 8vo. (1901.) 2s. 6d. net.
- Chemical Problems. By J. C. Foye. Fourth edition, 141 pp., 18mo, boards. (New York, 1898.) 2s. net.
- Primer of the Calculus. By E. S. Gould. Second edition, 24 illus., 122 pp., 18mo, boards. (New York, 1899.) 2s. net.

- Elementary Treatise on the Calculus for Engineering Students. By J. Graham. Third edition, 276 pp., crown 8vo. (FINSBURY TECHNICAL MANUAL.) (1905.) 7s. 6d.
- Manual of the Slide Rule. By F. A. Halsey. Second edition, 31 illus., 84 pp., 18mo, boards. (New York, 1901.) 2s. net.
- Rearm in Chemical and Physical Calculations. By C. J. T. Hanssen. 4to. (1897.) 6s. 6d. net.
- Algebra Self-Taught. By P. Higgs. Third edition, 104 pp., crown 8vo. (1903.) 2s. 6d.
- A Text-book on Graphic Statics. By C. W. Malcolm. 155 illus., 316 pp., 8vo. (New York, 1909.) 12s. 6d. net.
- Galvanic Circuit Investigated Mathematically. By G. S. Ohm. Translated by William Francis. 269 pp., 18mo, boards. (New York, 1891.) 2s. net.
- Elementary Practical Mathematics. By M. T. Ormsby. Second edition, 128 illus., xii + 110 pp., medium 8vo. (1911.) 5s. net.
- Elements of Graphic Statics. By K. Von Ott. Translated by G. S. Clarke. 95 illus., 128 pp., crown 8vo. (1901.) 5s
- Figure of the Earth. By F. C. Roberts. 18mo, boards. (New York.) 2s. net.
- Arithmetic of Electricity. By T. O'C. Sloane. Thirteenth edition, 5 illus., 162 pp., crown 8vo. (New York, 1901.) 4s. 6d. net.
- Graphic Method for Solving certain Questions in Arithmetic or Algebra. By G. L. Vose. Second edition, with 28 illus., 62 pp., 18mo, boards. (New York, 1902.) 2s. net.
- Problems in Electricity. A Graduated Collection comprising all branches of Electrical Science. By R. Weber. Translated from the French by E. A. O'Keefe. 34 illus., 366 pp., crown 8♥o. (1902.) 7s. 6d. net.

MECHANICAL ENGINEERING

Steam Engines and Boilers, etc.

- Engineers' Sketch Book of Mechanical Movements. By T. W. Barber. Fifth edition, 3,000 illus., 355 pp., 8vo. (1906.) ros. 6d. net.
- The Repair and Maintenance of Machinery. By T. W. Barber. 417 Llus., 476 pp., 8vo. (1895.) 10s. 6d.

- Practical Treatise on Mill Gearing. By T. Box. Fifth edition, 11 plates, 128 pp., crown 8vo. (1892.) 7s. 6d.
- The Mechanical Engineers' Price Book, 1913. Edited by G. Brooks. 176 pp., pocket size (6½ in. by 3¾ in. by ½ in. thick), leather cloth, with rounded corners. (1943.) 5s. net.
- Safety Valves. By R. H. Buell. Third edition, 20 illus., 100 pp., 18mo, boards. (New York, 1898.) 2s. net.
- Machine Design. By Prof. W. L. Cathcart.
 Part I. Fastenings. 123 illus., 291 pp., demy 8vo.
- (New York, 1903.) 12s. 6d. net.

 Chimney Design and Theory. By W. W. Christie. Second edition 54 illustration from Second Second
- edition, 5.4 illus., 192 pp., crown 8vo. (New York, 1902.)
 12s. 6d. net.
- Furnace Draft: its Production by Mechanical Methods. By W. W. Christie. 5 illus., 80 pp., 18mo, boards. (New York, 1906.) 2s. net.
- The Stokers' Catechism. By W. J. Connor. 63 pp., limp cloth. (1906.) is. net.
- Treatise on the use of Belting for the Transmission of Power. By J. H. Cooper. Fifth edition, 94 illus., 399 pp., demy 8vo. (New York, 1901.) 128. 6d. net.
- The Steam Engine considered as a Thermo-dynamic Machine. By J. H. Cotterill. Third edition, 39 diagrams, 444 pp., 8vo. (1896.) 15s.
- Fireman's Guide, a Handbook on the Care of Boilers. By K. P. Dahlstrom. Eleventh edition, fcap. 8vo, limp. (S. & C. Series, No. 16.) (New York, 1906.) 1s. 6d. net.
- Heat for Engineers. By C. R. Darling. Second edition, 110 illus., 430 pp., 8vo. (Finsbury Technical Manual.) (1912.) 12s. 6d. net.
- Diseases of a Gasolene Automobile, and How to Cure Them. By A. L. Dyke. 127 illus., 201 pp.; crown 8vo. (New York, 1903.) 6s. 6d. net.
- **Belt Driving.** By **G. Halliday.** 3 folding plates, 100 pp., 8vo. (1894.) 3s. 6d.
- Worm and Spiral Gearing. By F. A. Halsey. 13 plates, 85 pp., 18mo, boards. (New York, 1903.) 2s. net.
- Commercial Efficiency of Steam Boilers. By A. Hanssen, Large 8vo, sewed. (1898.) 6d.

- Corliss Engine. By J. T. Henthorn. Third edition, 23 illus., 95 pp., crown 8vo. (S. & C. Series, No. 23.) (New York, 1910.) 1s. 6d. net.
- **Liquid Fuel** for Mechanical and Industrial Purposes. By **E. A. Brayley Hodgetts.** 106 illus., 129 pp., 8vo. (1890.) 5s.
- Ele nentary Text-book on Steam Engines and Boilers. By J. H. Kinealy. Fourth edition, 106 illus., 259 pp., 8vo. (New York, 1903.) 8s. 6d. net.
- Centrifugal Fans. By J. H. Kinealy. 33 illus., 206 pp., fcap. 6vo, leather. (New York, 1905.) 12s. 6d. net.
- Mechanical Draft. By J. H. Kinealy. 27 original tables and 13 plates, 142 pp., crown 8vo. (New York, 1906.) 8s. 6d. net.
- The A B C of the Steam Engine, with a description of the Automatic Governor. By J. P. Lisk. 6 plates, crown 8vo. (S. & C. Series, No. 17.) (New York, 1910.) 1s. 6d. net.
- Valve Setting Record Book. By P. A. Low. 8vo, boards. 1s. 6d.
- The Lay-out of Corliss Valve Gears. By S. A. Moss. Second edition, 3 plates, 108 pp., 18mo, boards. (New York, 1906.) 2s. net.
- Steam Boilers, their Management and Working. By J. Peattie. Fifth edition, 35 illus., 230 pp., crown 8vo. (1906.) 4s. 6d. net.
- Treatise on the Richards Steam Engine Indicator. By C. T. Porter. Sixth edition, 3 plates and 73 diagrams, 285 pp., 8vo. (1902.) 9s.
 - Practical Treatise on the Steam Engine. By A. Rigg. Second edition, 103 plates, 378 pp., demy 4to. (1894.) £1 5s.
 - Power and its Transmission. A Practical Handbook for the Factory and Works Manager. By T. A. Smith. 76 pp., fcap. 8vo. (1910.) 2s. net.
 - Drawings for Medium Sized Repetition Work. By R. D. Spinney. With 47 illus., 130 pp., 8vo. (1909.) 3s. 6d. net.
- Slide Valve Simply Explained. By W. J. Tennant. Revised by J. H. Kinealy. 41 illus., 83 pp., crown 8vo. (New York, 1899.) 4s. 6d. net.
- Shaft Governors. By W. Trinks and C. Hoosum. 27 illus., 97 pp., 18mo, poards. (New York, 1905.) 2s. net.

- Treatise on the Design and Construction of Mill Buildings. By H. G. Tyrrell. 652 illus., 490 pp., 8vo. (New, York, 1911.) 178. net.
- Slide and Piston Valve Geared Steam Engines. By W. H. Uhland. 47 plates and 314 illus., 155 pp. Two vols., tolio, half morocco. (1882.) £1 16s.
- How to run Engines and Boilers. By E. P. Watson. Fifth edition, 31 illus., 160 pp., crown 8vo. (New York, 1904.) 38, 6d.
- Position Diagram of Cylinder with Meyer Cut-off. By W. H. Weightman. On card. (New York.) is. net.
- Practical Method of Designing Slide Valve Gearing. By E. J. Welch. 69 illus, 283 pp., crown 8vo. (1890.) 6s.
- Elements of Mechanics. By T. W. Wright. Eighth edition, illustrated, 382 pp., 8vo. (New York, 1909.) 108, 6d, net.

METALLURGY

Iron and Steel Manufacture

- Life of Railway Axles. By T. Andrews. 8vo, sewed. (1895.) 1s.
- Microscopic Internal Flaws in Steel Rails and Propeller Shafts. By T. Andrews. 8vo, sewed. (1896.) 1s.
- Microscopic Internal Flaws, Inducing Fracture in Steel. By T. Andrews. 8vo, sewed. (1896.) 2s.
- Practical Alloying. A compendium of Alloys and Processes for Brassfounders, Metal Workers, and Engineers. By John F. Buchanan. 41 illus., 205 pp., 8vo. (New York, 1911.) 10s. 6d. net.
- Brassfounders' Alloys. By J. F. Buchanan. 23 illus., viii + 129 pp., crown 8vo. (1905.) 4s. 6d. net.
- The Moulder's Dictionary (Foundry Nomenclature). By J. F. Buchanan. New impression, 26 illus., viii + 225 pp., crown 8vo. (1912.) 3s. net.
- American Standard Specifications for Steel. By A. L. Colby. Second edition, revised, 103 pp., crown 8vo. (New York, 1902.) 5s. net.
- Galvanized Iron: its Manufacture and Uses. By J. Davies. 139 pp., 8vo. (1899.) 5s. net.
- Management of Steel. By G. Ede. Seventh edition, 216 pp., crown 8vo. (1903.) 5s.

- The Frodair Handbook for ironfounders. 100 pp., 12mo. (1914.) 2s. net.
- Manufacture of Iron and Steel. By H. R. Hearson. 21 illus., xii + 103 pp., 8vo. (1912.) 4s. 6d. net.
- Cupola Furnace. By E. Kirk. Third edition, 106 illus., 484 pp., 8vo. (New York, 1910.) 158, net.
- Practical Notes on Pipe Founding. By J. W. Macfarlane. 15 plates, 148 pp., 8vo. (1888.) 12s. 6d.
- Atlas of Designs concerning Blast Furnace Practice. By M. A. Pavloff. 127 plates, 14 in. by 10½ in. oblong, sewed. (1902.) £1 is. net.
- Album of Drawings relating to the Manufacture of Open Hearth Steel. By M. A. Pavloff.
 - Part I. Open Hearth Furnaces. 52 plates, 14 in. by 101 in. oblong folio, in portfolio. (1904.) 12s. net.
- Metallography Applied to Siderurgic Products. By H. Savoia. Translated by R. G. Corbet. 94 illus., 180 pp., crown 8vo. (1910.) 4s. 6d. net.
- Modern Foundry Practice. By J. Sharp. Second edition, new impression, 272 illus., 759 pp., 8vo. (1911.) £1 µs. net.
- How to Make Converter Steel Castings. By A. Simonson. 23 illus., v1 + 40 pp., 8vo. (New York, 1910.) 4s. 6d. net.
- Roll Turning for Sections in Steel and Iron. By A. Spencer. Second edition, 78 plates, 4to. (1894.) f. 1 108.

METRIC TABLES

- French Measure and English Equivalents. By J. Brook. Second edition, 80 pp., fcap. 32mo, roan. (1913.) is. net.
- A Dictionary of Metric and other useful Measures. By L. Clark. 113 pp., 8vo. (1891.) os.
- English Weights, with their Equivalents in kilogrammes. By F. W. A. Logan, 96 pp., fcap. 32mo, roan. (1906.)1s. net.
- Metric Weights with English Equivalents. By H. P. McCartney. 84 pp., fcap. 32mo, roan. (1907.) 1s. net.
- Metric Tables. By Sir G. L. Molesworth. Fourth edition, 95 pp., royal Jano. (1909) 28, net.

Tables for Setting out Curves from 200 metres to 4,000 metres by tangential angles. By **H. Williamson.** 4 illur., 69 pp., 18mo. (1908.) 2s. net.

MINERALOGY AND MINING

- **Rock Blasting.** By **G. G. Andre.** 12 plates and 56 illùs, in text, 202 pp., 8vo. (1878.) 5s.
- Winding Plants for Great Depths. By H. C. Behr. In two parts. 8vo, sewed. (1902.) £2 2s. net.
- Practical Treatise on Hydraulic Mining in California. By A. J. Bowie, Junr. Tenth edition, 73 illus., 313 pp., royal 8vo. (New York, 1905.) [1 1s. net.
- Tables for the Determination of Common Rocks. By O. Bowles. 64 pp., 18mo, boards. (Van Nostrand Series, No. 125.) (New York, 1910.) 2s. net.
- Manual of Assaying Gold, Silver, Copper and Lead Ores. By W. L. Brown. Twelfth edition, 132 illus., 589 pp., crown 8vo. (New York, 1907.) 108. 6d. net.
- Fire Assaying. By E. W. Buskett. 69 illus., 105 pp., crown 8vo. (New York, 1907.) 4s. 6d. net.
- Tin: Describing the Chief Methods of Mining, Dressing, etc. By A. G. Charleton. 15 plates, 83 pp., crown 8vo. (1884.) 12s. 6d.
- Gold Mining and Milling in Western Australia, with Notes upon Telluride Treatment, Costs and Mining Practice in other Fields. By A. G. Charleton. 82 illus, and numerous plans and tables, 648 pp., super royal 8vo. (1903.) £1 5s. net.
- Miners' Geology and Prospectors' Guide. By G. A. Corder. 29 plates, 224 pp., crown 8vo. (1907.) 5s. net.
- Blasting of Rock in Mines, Quarries, Tunnels, etc. By A. W. and Z. W. Daw. Second edition, 90 illus., 316 pp., demy 8vo. (1909.) 15s. net.
- Handbook of Mineralogy; determination and description of Minerals found in the United States. By J. C. Foye. 180 pp., 18mo, boards. (New York, 1886.) 2s. net.
- Our Coal Resources at the End of the Nineteenth Century. By Prof. E. Hull. 157 pp., demy 3vo. (1897.) 6s.
- Hydraulic Gold Miners' Manual. By T. S. G. Kirkpatrick. Second edition, 12 illus., 46 pp., crown 8vo. (1987.) 4s.
- Economic Mining. By G. G. W. Lock. 175 illus., 680 pp., 8vo. (1895.) 10s. 6d. net.

- Gold Milling: Principles and Practice. By C. G. W. Lock. 200 illus., 850 pp., demy 8vo. (1901.) fi is. net.
- Mining and Ore-Dressing Machinery. By C. G. W. Lock. 639 illus., 466 pp., super royal 4to. (1890.) 41 5s.
- Miners' Pocket Book. By C. G. W. Lock. Fifth edition, 233 illus., 624 pp., fcap. 8vo, leather, gilt edges. (1908.) 10s. 6d. net.
- Chemistry, Properties and Tests of Precious Stones. By J. Mastin. 114 pp., fcap. 16mo, limp leather, gilt top. (1911.) 2s. 6d. net.
- Tests for Ores, Minerals and Metals of Commercial Value. By R. L. McMechen. 152 pp., 12mo. (New York, 1907.) 5s. 6d. net.
- Practical Handbook for the Working Miner and Prospector, and the Mining Investor. By J. A. Miller. 34 illus., 234 pp., crown 8vo. (1897.) 7s. 6d.
- Theory and Practice of Centrifugal Ventilating Machines. By D. Murgue. 7 illus., 81 pp., 8vo. (1883.) 58.
- **Examples of Coal Mining Plant.** By J. Povey-Harper. Second edition, 40 plates, 26 m. by 20 in. (1895.) £4.4s. net.
- Examples of Coal Mining Plant, Second Scries. By J. Povey-Harper. 10 plates, 26 in. by 20 in. (1902.), £1 12s. 6d. net.

MODELS AND MODEL MAKING

- How to Build a Model Yacht. By H. Fisher. Numerous illustrations, 50 pp., 4to. (New York, 1902.) 4s. 6d. net.
- Model Engines and Small Boats. By N. M. Hopkins. 50 illus., viii+74 pp., crown 8vo. (New York, 1898.) 5s. 9d. net.
- The Gyroscope, an Experimental Study. By V. E. Johnson. 34 illus., 40 pp., crown 8vo, limp. (S. & C. Series, No. 22.) (1911_t) is. 6d. net.
- The Model Vaudeville Theatre. By N. H. Schneider. 34 illus., 90 pp., crown 8vo, limp. (S. & C. Series, No. 15.) (New York, 1910.) 1s. 6d.
- Electric Toy-Making. By T. O. Sloane. Fifteenth edition, 70 illus., 183 pp., crown 8vo. (New York, 1903.) 4s. 6d. net.
- 'Model-Steam Engine Design. By R. M. De Vignier. 34 illus., 94 pr. crewn 8vo. limp. (S. &. C. Series, No. 9.) (New York, 1507.) 18. 6d. net.

Small Engines and Boilers. By E. P. Watson. 33 illus., viii + 108 pp., crown 8vo. (New York, 1899.) 55.6d.,net.

ORGANIZATION

Accounts, Contracts and Management

- Organization of Gold Mining Business, with Specimens of the Departmental Report Books and the Account Books. By Nicol Brown. Second edition, 220 pp., fcap. folio. (1903.) £1 5s. net.
- Cost Keeping and Management Engineering. A Treatise for those engaged in Engineering Construction. By H. P. Gillette and R. T. Dana. 184 illus., 346 pp., 8vo. (New York, 1909.) 158, net.
- Manual of Engineering Specifications and Contracts. By L. M. Haupt. Eighth edition, 338 pp., 8vo. (New York, 1900.) 128. 6d net.
- Handbook on Railway Stores Management. By W. O. Kempthorne. 268 pp., demy 8vo. (1907.) 108, 6d. net.
- Depreciation of Factories, Municipal, and Industrial Undertakings, and their Valuation. By E. Matheson. Fourth edition, 230 pp., 8vo. (1910.) 10s. 6d. net.
- Aid Book to Engineering Enterprise. By E. Matheson. Third edition, 916 pp., 8vo, buckram. (1898.) £1 4s.
- Office Management. A handbook for Architects and Civil Engineers. By W. Kaye Parry. New impression, 187 pp., . medium 8vo. (1908.) 5s. net.
- Commercial Organization of Engineering Factories. By H. Spencer. 92 illus., 221 pp., 8vo. (1907.) 10s. 6d. nct.

PHYSICS

Colour, Heat and Experimental Science

- The Entropy Diagram and its Applications. By M. J. Boulvin. 38 illus., 82 pp., demy 8vo. (1898.) 5s.
- Physical Problems and their Solution. By A. Bourgougnon. 224 pp., 18mo, boards. (New York, 1897.) 2s. net.
- Heat for Engineers. By C. R. Darling. Second edition, 110 illus., 430 pp., 8vo. (FINSBURY TECHNICAL MANUAL.) (1912.) 12s. 6d. net.

- The Colourist. A method of determining colour harmony. By J. A. H. Hatt. 2 coloured plates, 80 pp., 8vo. (New York, 1908.) 6s. 6d. net.
- Engineering Thermodynamics. By C. F. Hirschfeld. 22 illus., 157 pp., 18mo, boards. (New York, 1907.) 2s. net.
- Experimental Science: Elementary, Practical and Experimental Physics. By G. M. Hopkins. Twenty-third edition, 920 illus., 1,100 pp., large 8vo. (New York, 1902.) £1 1s. net.
- Reform in Chemical and Physical Calculations. By C. J. T. Hanssen. Demy 4to. (1897.) 6s. 6d. net.
- Introduction to the Study of Colour Phenomena. By J. W.
 Lovibond. 10 hand coloured plates, 48 pp., 8vo. (1905)
 5s. net.
- Practical Laws and Data on the Condensation of Steam in Bare Pipes; to which is added a Translation of Peclet's Theory and Experiments on the Transmission of Heat through Insulating Materials. By C. P. Paulding. 184 illus., 102 pp., demy 8vo. (New York, 1901.) 8s. 6d. net.
- **The Energy Chart.** Practical application to reciprocating steam-engines. By Captain **H. R. Sankey.** 157 illus., 170 pp., 8vo. (1907.) 7s. 6d. net.

PRICE BOOKS

- The Mechanical Engineers' Price Book, 1913. By G. Brooks. 200 pp., pocket size (6½ in. by 3¾ in. by ½ in. thick), leather cloth, with rounded corners. (1913.) 5s. net.
- Approximate Estimates. By T. E. Coleman. Third edition, 481 pp., oblong 32mo, leather. (1907.) 5s. net.
- The Civil Engineers' Cost Book. By Major T. E. Coleman. xii + 280 pp., pocket size $(6\frac{1}{2}$ in. by $3\frac{3}{4}$ in.), leather cloth. (1912.) 5s. net.
- Railway Stores Price Book. By W. O. Kempthorne. 500 pp., demy 8vo. (1909.) 10s. 6d. net.
- Handbook of Cost Data for Contractors and Engineers. By H. P. Gillette. 1,854 pp., crown 8vo, leather, gilt edges. (New York, 1911.) £1 1s. net.
- Spons' Architects' and Builders' Pocket Price-Book and Diary, 1912. Edited by Clyde Young. Revised by Stanford M. Brooks. Illustrated, 239 pp., green leather cloth. With Diary showing a week at an opening. (Size 6½ in. by 3¼ in. i.y.½ in. 'hick.) Issued annually. 2s. 6d. net.

RAILWAY ENGINEERING AND MANAGEMENT

- Practical Hints to Young Engineers Employed on Indian Railways. By A. W. C. Addis. 14 illus., 154 pp., 12mo. (1910.) 3s. 6d. net.
- Field and Office Tables, specially applicable to Rair Jads. By C. F. Allen. 293 pp., 16mo, leather. (New York, 1903.) 8s. 6d. net.
- Up-to-date Air Brake Catechism. By R. H. Blackall. Twenty-third edition, 5 coloured plates, 96 illus., 305 pp., crown 8vo. (New York, 1908) 8s. 6d. net.
- Prevention of Railroad Accidents, or Safety in Railroading. By Geo. Bradshaw. 64 illus., 173 pp., square crown 8vo. (New York, 1912.) 2s. 6d. net.
- Simple and Automatic Vacuum Brakes. By C. Briggs, G.N.R. 11 plates, 8vo. (1892.) 4s.
- Notes on Permanent-way Material, Plate-laying, and Points and Crossings. By W. H. Cole. Sixth edition, revised, 44 illus. in 39 plates, 203 pp., crown &vo. (1912.) 7s. 6d. roct.
- Statistical Tables of the Working of Railways in various countries up to the year 1904. By J. D. Diacomidis. Second edition, 84 pp., small folio, sewed. (1906.) 16s. net.
- Locomotive Breakdowns, Emergencies and their Remedies. By Geo. L. Fowler, M.E., and W. W. Wood. Fifth edition, 92 illus., 266 pp., 12mo. (New York, 1911.) 4s. 6d. net.
- Permanent-way Diagrams. By F. H. Frere. Mounted on linen in cloth covers. (1908.) 3s. net.
- Formulæ for Railway Crossings and Switches. By J. Glover. 9 illus., 28 pp., royal 32mo. (1896.) 2s. 6d.
- Setting out of Tube Railways. By G. M. Halden. 9 plates, 46 illus., 68 pp., crown 4to. (1907.) 10s. 6d. net.
- Railway Engineering, Mechanical and Electrical. By J. W. C. Haldane. New edition, 1.41 illus., xx + 583 pp., 8vo. (1908.) 15s.
- The Construction of the Modern Locomotive. By G. Hughes. 300 illus., 261 pp., 8vo. (1894.) 9s.
- Practical Ilints for Light Railways at Home and Abroad, By F. R. Johnson. 6 plates, 31 pp., crown 8vo. (1896.) 2s. 6d.

- Handbook on Railway Stores Management. By W. O. Kempthorne. 268 pp., demy 8vo. (1907.) 10s. 6d. net.
- Railway Stores Price Book. By W. O. Kempthorne.
- Railroad Location Surveys and Estimates. By F. Lavis. 68 illus, 270 pp., 8vo. (New York, 1906.) 12s. 6d. net.
- Piokering. By F. Shelford. Illustrated, 88 pp., crown 8vo. (1909.) 3s. net.
- Handbook on Railway Surveying for Students and Junior Engineers. By B. Stewart. 55 illus., 98 pp., crown 8vo. (1909.) 2s. 6d. net.
- Modern British Locomotives. By A. T. Taylor. 100 diagrams of principal dimensions, 118 pp., oblong 8vo. (1907.) 4s. 6d. net.
- Locomotive Slide Valve Setting. By C. E. Tully. Illustrated, 18mo. 1s. net.
- The Railway Goods Station. By F. W. West. 23 illus., xv + 192 pp., crown 8vo. (1912.) 4s. 6d. net.
- The Walschaert Locomotive Valve Gear. By W. W. Wood.

 4 plates and set of movable cardboard working models of
 the valves, 193 pp., crown 8vo. (New York, 1912.) 6s. 6d.
 net.
- The Westinghouse E.T. Air-Brake Instruction Pocket Book. By W. W. Wood. 48 illus., including many coloured plates, 242 pp., crown 8vo. (New York, 1909.) 8s. 6d. net.

SANITATION, PUBLIC HEALTH AND MUNICIPAL ENGINEERING

- Sewers and Drains for Populous Districts. By J. W. Adams. Ninth edition, 81 illus., 236 pp., 8vo. (New York, 1902.) 20s. 6d. net.
- Engineering Work in Public Buildings. By R. O. Allsop. 77 illus., ix + 158 pp., demy 4to. (1912.) 12s. 6d. net.
- Public Abattoirs, their Planning. Design and Equipment. By R. S. Ayling. 33 plates, 100 pp., demy 4to. (1908.) 8s. 6d. net.
- Sewage Purification. By E. Bailey-Denton. 8 plates, 44 pp., 85. '396.) 5s.

- 40 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- Water Supply and Sewerage of Country Mansions and Estates. By E. Bailey-Denton. 76 pp., crown 8vo (1901.) 2s. 6d. net.
- Sewerage and Sewage Purification. By M. N. Baker. Second edition, 144 pp., 18mo, boards. (New York, 1905.)
- Sewage Irrigation by Farmers. By R. W. P. Birch. of 8vo, sewed. (1878.) 2s. 6d.
- Bacteriology of Surface Waters in the Tropics. By W. W. Clemesha. viii + 161 pp., 8vo. (Calcutta, 1912.) 7s. 6d net.

 Sanitary House Drainage, its Principles and Practice. By
- T. E. Coleman. 98 illus., 206 pp., crown 8vo. (1896.) 6s. Stable Sanitation and Construction. By T. E. Coleman. 183 illus., 226 pp., crown 8vo. (1897.) 6s.
- Public Institutions, their Engineering, Sanitary and other Apphances. By F. Colyer. 231 pp., 8vo. (1889.) 28. net.
- Discharge of Pipes and Culverts. By P. M. Crosthwaite.

 Large folding sheet in case. 2s. 6d. net.
- A Complete and Practical Treatise on Plumbing and Sanitation, By G. B. Davis and F. Dye. 2 vols., 637 illus. and 21 folding plates, 830 pp., 4to, cloth. (1899.) £1 10s. net.
- Vol. I. Fourth edition, 768 illus., 355 pp., royal 8vo. (1905.) 7s. 6d. net.
 - Vol. H. Second edition, 953 illus., 805 pp. (1905.) 10s. 6d. net.
 Vol. III. 313 illus., 204 pp. (1905.) 5s. net.
 - Conservancy, or Dry Sanitation versus Water Carriage. By J. Donkin. 7 plates, 33 pp., 8vo, sewed. (1906.) 1s.
- net.

 Sewage Disposal Works. By W. C. Easdale. 160 illus., 264 pp., 8vo. (1910.) 10s. 6d. net.
- House Drainage and Sanitary Plumbing. By W. P. Gerhard. Tenth edition, 6 illus., 231 pp., 18mo, boards. (New York, 1902.) 2s. net.
- Central Station Heating. By B. T. Gifford. 37 illus., 208 pp., 8vo., leather. (New York, 1912.) 17s. net.

- Housing and Town Planning Conference. Report of Conference held by the Institution of Municipal and County Engineers. Edited by T. Cole, Secretary. 30 plates, 240 pp., demy 8vo. (1911.) 10s. 6d. net.
- Engineering Work in Towns and Cities. By E. McCulloch. iilus., 502 pp., crown 8vo. (New York, 1908.) 12s. 6d. het.
- The Treatment of Septic Sewage. By G. W. Rafter. 137 pp., 18mo, boards. (New York, 1904.) 2s. net.
- Reports and Investigations on Sewer Air and Sewer Ventilation. By R. H. Reeves. 8vo, sewed. (1894.) 1s.
 - The Law and Practice of Paving Private Street Works. By W. Spinks. Fourth edition, 256 pp., 8vo. (1904.) 12s. 6d. net.

STRUCTURAL DESIGN

(See Bridges and Roofs)

TELEGRAPH CODES

- New Business Code. 320 pp., narrow 8vo. (Size $4\frac{3}{4}$ in. by $7\frac{3}{4}$ in. and $\frac{1}{2}$ in. thick, and weight 10 oz.) (New York, 1909.) f_1 1s. net.
- Miners' and Smelters' Code (formerly issued as the Master Telegraph Code). 448 pp., 8vo, limp leather, weight 14 oz. (New York, 1899.) £2 10s. net.
- Billionaire Phrase Code, containing over two million sentences coded in single words. 56 pp., 8vo, leather. (New York, 1908.) 6s. 6d. net.

WARMING AND VENTILATION

- Heat for Engineers. By C. R. Darling. Second edition, 110 illus., 430 pp., 8vo. (FINSBURY TECHNICAL MANUAL.) (1912.) 12s. 6d. net.
- Hot Water Supply. By F. Dye. Fifth edition, new impression, 48 illus., viii + 86 pp., 8vo. (1912.) 3s. net.
- A Practical Treatise upon Steam Heating. By F. Dye. 120 illus., 246 pp., 8vo. (1901.) 10s. net.
- Practical Treatise on Warming Buildings by Hot Water. By F. Dye. A. ailus., 319 pp., 8vo. (1905.) 8s. 6d. net.

- 42 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- Central Station Heating. By B. T. Gifford. 37 illus., 208 pp., 8vo, leather. (New York, 1912.) 178. Fet.,
- Charts for Low Pressure Steam Heating. By J. H. Kinealy. Small folio. (New York.) 48, 6d.
- Formulæ and Tables for Heating. By J. H. Kinealy. 18 illus., 53 pp., 8vo. (New York, 1899.) 3s. 6d.
- Centrifugal Fans. By J. H. Kinealy. 33 illus., 206 pp., fcap. 8vo, leather. (New York, 1905.) 12s. 6d. net.
- Mechanical Draft. By J. H. Kinealy. 27 original tables and 13 plates, 142 pp., crown 8vo. (New York, 1906.) 8s. 6d. net.
- Theory and Practice of Centrifugal Ventilating Machines. By D. Murgue. 7 illus., 81 pp., 8vo. (1883.) 5s.
- Mechanics of Ventilation. By G. W. Rafter. Second edition, 143 pp., 18mo, boards. (New York, 1896.) 28, net.
- Principles of Heating. By W. G. Snow. New edition, 59 illus., xii + 224 pp., 8vo. (New York, 1912.) 98, net.
- Furnace Heating. By W. G. Snow. Fourth edition, 52 illus., 216 pp., 8vo. (*New York*, 1909.) 6s. 6d. net.
- Vertilation of Buildings. By W. G. Snow and T. Nolan. 83 pp., 18mo, boards. (New York, 1906.) 2s. net.
- Heating Engineers' Quantities. By W. L. White and G. M. White. 4 plates, 33 pp., folio. (1910.) 10s. 6d. net.

WATER SUPPLY

(See also **Hydraulics**)

- Potable Water and Methods of Testing Impurities. By M. N. Baker. 97 pp., 18mo, boards. (New York, 1905.) 2s. net.
- Manual of Hydrology. By N. Beardmore. New impression, 18 plates, 384 pp., 8vo. (1906.) 10s. 6d. net.
- Boiler Waters, Scale, Corrosion and Fouling. By W. W. Christie. 77 illus., 235 pp., 8vo. (New York, 1907.) 128, 6d. net.
- Water Softening and Purification. By H. Collet. Second edition, 6 illus., 170 pp., crown 8vo. (1908.) 5s. net.
- Treatise on Water Supply, Drainage and Sanitary Appliances, of Residences. By F. Colyer. 100 pp., crown 8vo. (1899.) 1s. 6d. net.

- Purification of Public Water Supplies. By J. W. Hill. 314 pp., 8vo. (New York, 1898.) 10s. 6d.
- Well Boring for Water, Brine and Oil. By C. Isler. Second edition, 105 illus., 296 pp., 8vo. (1911.) 10s. 6d. net.
- Method of Measuring Liquids Flowing through Pipes by means of Meters of Small Calibre. By Prof. G. Lange. P plate, 16 pp., 8vo, sewed. 6d. net.
- On Artificial Underground Water. By G. Richert. 16 illus., 33 pp., 8vo, sewed. (1900.) 1s. 6d. net.
- Notes on Water Supply in new Countries. By F. W. Stone. 18 plates, 42 pp., crown 8vo. (1888.) 58.
 - The Principles of Waterworks Engineering. By J. H. T. Tudsbery and A. W. Brightmore. Third edition, 13 folding plates, 130 illus., 447 pp., demy 8vo. (1905.) £1 is. net.

WORKSHOP PRACTICE

For Art Workers and Mechanics

- A Handbook for Apprenticed Machinists. By O. J. Beale. Second edition, 89 illus., 141 pp., 16mo. (New York, 1901.) 2s. 6d. net.
- Practice of Hand Turning. By F. Campin. Third edition, 99 illus., 307 pp., crown 8vo. (1883.) 3s. 6d.
- Artistic Leather Work. By E. Ellin Carter. 6 plates and 21 illus, in text, xii + 51 pp., crown 8vo. (1912.) 2s. 6d. net.
- Calculation of Change Wheels for Screw Cutting on Lathes. By D. de Vries. 46 illus., 83 pp., 8vo. (1908.) 3s. net
- Milling Machines and Milling Practice. By D. de Vries. 536 illus., 464 pp., medium 8vo. (1910.) 14s. net.
- French-Polishers' Manual. By a French-Polisher. New impression, 31 pp., royal 32mo, sewed. (1912.) 6d. net.
- Art of Copper-Smithing. By J. Fuller. Fourth edition, 483 illus., 319 pp., royal 8vo. (New York, 1911.) 12s. 6d. net.
- Hand Forging and Wrought Iron Ornamental Ironwork.

 By T. F. Googerty. 122 illus., 197 pp., crown 8vo. (New York, 1912.) 4s. 6d. net.
- Saw Filing and Management of Saws. By R. Grimshaw.
 New edition, contract and sample of Saws. By R. Grimshaw.
 New Pork, 1906. 4s. 6d. net.

- 44 E. & F. N. SPON, Ltd., 57, HAYMARKET, LONDON, S.W.
- Paint and Colour Mixing. By A. S. Jennings. Fourth edition, 14 coloured plates, 190 pp., 8vo. (1910.) 5s.
- The Mechanician: a Treatise on the Construction and Manipulation of Tools. By C. Knight. Fifth edition, 96 plates, 397 pp., 4to. (1897.) 18s.
- Turner's and Fitter's Pocket Book. By J. La Nicca. idmo, sewed. 6d.
- Tables for Engineers and Mechanics, giving the values of the different trains of wheels required to produce Screws of any pitch. By Lord Lindsay. Second edition, royal 8vo, oblong. 2s.
- Screw-cutting Tables. By W. A. Martin. Seventh edition, royal 8vo, oblong. 1s. net.
- Metal Plate Work, its Patterns and their Geometry, for the use of Tin, Iron and Zinc Plate Workers. By C. T. Millis. Fourth edition. New impression, 280 diagrams, xvi + 456 pp., crown 8vo. (1912.) 98.
- The Practical Handbook of Smithing and Forging. Engineers' and General Smiths' Work. By T. Moore. New impression, 401 illus., 248 pp., crown 8vo. (1912.) 5s. net.
- Modern Machine Shop Construction, equipment and management. By O. E. Perrigo. 208 illus., 343 pp., crown 4to. (New York, 1906.) £1 1s. net.
- Turner's Handbook on Screw-cutting, Coning. etc. By W. Price. New impression, Icap. 8vo. (1912.) 6d.
- net.

 Introduction to Eccentric Spiral Turning. By H. C.
 Robinson. 12 plates, 23 illus., 48 pp., 8vo. (1906.)
- Manual of Instruction in Hard Soldering. By H. Rowell. Sixth edition, 7 illus., 66 pp., crown 8vo. (New York, 1910.)

4s. 6d. net.

- Forging, Stamping, and General Smithing. By B. Saunders. 728 illus., ix + 428 pp., demy 8vo. (1912.) £1 is. net.
- Pocket Book on Boilermaking, Shipbuilding, and the Steel and Iron Frades in General. By M. J. Sexton. Sixth edition, new impression, 85 illus., 319 pp., royal 32mo, roan, gilt edges. (1912.) 5s. net.

- Power and its Transmission. A Practical Handbook for the l'actory and Works Manager. By T. A. Smith. 76 pp., fcap. 8vo. (1910.) 2s. net.
- Spons' Mechanics' Own Book: A Manual for Handicraftsmen and Amateurs. Sixth edition. New impression, 1,430 illus., 720 pp., demy 8vo. (1912.) 6s.

 Ditto ditto half French morocco, 7s. 6d.
- Spons' Workshop Receipts for Manufacturers, Mechanics and Scientific Amateurs. New and thoroughly revised edition, crown 8vo. (1909.) 3s. each net.
 Vol. I. Acetylene Lighting to Drying. 223 illus., 532 pp.
 Vol. II. Dyfing to Japanning. 259 illus., 540 pp.
 Vol. III. Jointing Pipes to Pumps. 257 illus., 528 pp.
 - Vol. III. DYFING to JAPANNING. 250 mus., 540 pp. Vol. III. Jointing Pipes to Pumps. 257 illus., 528 pp. Vol. IV. Rainwater Separators to Wire Ropes. 321 illus., 540 pp.
 - **Gauges at a Glance.** By **T. Taylor.** Second edition, post 8vo, oblong, with tape converter. (1900.) 5s. net.
 - Simple Soldering, both Hard and Soft. By E. Thatcher. 52 illus., 76 pp., crown 8vo. (S. & C. Series, No. 18.) (New York, 1910.) 18. 6d. net.
 - **The Modern Machinist.** By **J. T. Usher.** Fifth edition, 257 illus., 322 pp., 8vo. (*New York, 1904.*) 10s. 6d. net.
- Knots, Splices, and Rope-Work. By A. H. Verrill. 148 illus., 102 pp., 12mo. (New York, 1912.) 3s. net.
 - Practical Wood Carving. By C. J. Woodsend. 108 illus., 86 pp., 8vo. (New York, 1897.) 4s. 6d. net.
 - American Tool Making and Interchangeable Manufacturing. By J. W. Woodworth. 600 illus., 544 pp., demy 8vo. (New York, 1905.) 17s. net.

USEFUL TABLES

- See also Curve Tables, Earthwork, Foreign Exchange, Interest Tables, Logarithms, and Metric Tables.
- Weights and Measurements of Sheet Lead. By J. Alexander. 32mo, roan. 1s. 6d. net.
- Barlow's Tables of Squares, Cubes, Square Roots, Cube Loots and Reciprocals, of all Integer Numbers from 1 to 10,000. 200 pp., crown 8vo, leather cloth. 4s. net.
- Tables of Squares. Of every foot, inch and $\frac{1}{16}$ of an inch from $\frac{1}{16}$ of an inch to 50 feet. By E. E. Buchanan. Eleventh edition, 102 pp., 10mo. (New York, 1912.) 4s. 6d. act.
- Land Area Tables. By W. Codd. On sheet mounted on linen, in cloth case with explanatory pamphlet. (1920.) 3s.,6d.
- Tables of some of the Principal Speeds occurring in Mechanical Engineering, expressed in Metres per second. By K. Keerayeff. 18mo, sewed. 6d. net.
- Calculating Scale. A Substitute for the Slide Rule. By W. Knowles. Crown 8vo, leather. 1s. net.
- **Planimeter Areas.** Multipliers for various scales. By **H. B. Molesworth.** Folding sheet in cloth case. 1s. net.
- **Tables of Seamless Copper Tubes.** By **I. O'Toole.** 69 pp., oblong fcap. 8vo. (1908.) 3s. 6d. net.
- Steel Bar and Plate Tables. Giving Weight per Lineal Foot of all sizes of L and T Bars, Flat Bars, Plates, Square, and Round Bars. By E. Read. On large folding card. (1911.)
- Rownson's Iron Merchants' Tables and Memoranda. Weight and Measures. 86 pp., 32mo, leather. 3s. 6d.
- Spons' Tables and Memoranda for Engineers. By J. T.
 Hurst, C.E. Twelfth edition, 278 pp., 64mo, roan, gilt edges. (1907.) 1s. net.
 Ditto ditto in celluloid case, 1s. 6d. net.
- Optical Tables and Data, for the use of Opticians. By Prof. S. P. Thompson. Second edition, 130 pp., oblong 8vo. (1907.) 6s. net.
- Traverse Table, showing Latitudes and Departure for each Quarter degree of the Qudrant, and for distances from 1 to 100, etc. 18mo, boards. 2s. net.

- Fifty-four Hours' Wages Calculator. By H. N. Whitelaw. Second edition, 79 pp., 8vo. 2s. 6d. net.
- Wheef Gearing. Tables of Pitch Line Diameters, etc. By A. Wildgoose and A. J. Orr. 175 pp., fcap. 32mo. (1903.) 2s. net.

MISCELLANEOUS

- F. J. B. Cordeiro. 35 illus., 129 pp., crown 4to. (New York, 1910.) 10s. 6d. net.
 - Forular Engineering. By F. Dye. 704 illus., 477 pp., crown 4to. (1895.) 5s. net.
 - **The Phonograph,** and how to construct it. By **W. Gillett.** 6 tolding plates, 87 pp., crown 8vo. (1892.) 5s.
 - Engineering Law. By A. Haring. Demy 8vo, cloth. (New York.)
 Vol. I. The Law of Contract. 518 pp. (1911.)
 178, net.
 - The Gyroscope, an Experimental Study. By V. E. Johnson. 34 illus., 40 pp., crown 8vo. (S. & S. SERIES, No.
 - Particulars of Dry Docks, Wet Docks, Wharves, etc., on the River Thames. By C. H. Jordan. Second edition, 7 coloured charts, 103 pp., oblong 8vo. (1904.) 2s. 6d. net.

22.) (1911.) Is. 6d. net.

- New Theories in Astronomy. By W. Stirling. 335 pp., demy 8vo. (1906.) 8s. 6d. net.
- The American Hardware Store. A Manual of approved methods of arranging and displaying hardware. By R. R. Williams. 500 illus., 448 pp., royal 8vo. (New York, 1896.) 2s. 6d. net.
- Inventions, How to Protect, Sell and Buy Them. By F. Wright. 118 pp., crown 8vo. (S. & C. Series, No. 10.) (New York, 1908) 1s. 6d. net.

The Journal of the Iron and Steel Institute.

Edited by G. C. LLOYD, Secretary. Published Half-yearly, 8vo. 18s. net.

Carnegie Scholarship Memoirs.

Published Annually, 8vo.

The Journal of the Institution of Electrical Engineers.

Edited by P. F. ROWELL, Secretary.

The Proceedings of the Institution of Municipal and County Engineers.

Edited by Thomas Cole, Assoc.M.Inst.C.E. Secretary. Published Annually, 8vo. 21s. net.

The Transactions of the Institution of Mining and Metallurgy.

Edited by C. McDermid, Secretary. Published Annually, boards, 21s. net, or half-bound, 25s. net.

Transactions of the Institution of Gas Engineers.

Edited by Walter T. Dunn, Secretary.
Published Annually, 8vo. 10s. 6d. net.

Proceedings of the International Association for Testing Materials.

(English Edition.)

Transactions of the American Institute of Chemical Engineers.

Published Annually, 8vo. 3os. net.

Printed by Butler & Tanner, Frome and I .- don.